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# Stein estimation in the Conway-Maxwell Poisson model with correlated regressors



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### ABSTRACT

The Poisson regression model (PRM) is widely used for count data, applicable when the response variable follows a Poisson distribution with equal dispersion. The Conway-Maxwell Poisson regression model (COMPRM) is more flexible and can handle both under-dispersion and over-dispersion. However, the COMPRM may involve correlated regressors, leading to multicollinearity, which makes the maximum likelihood estimator (MLE) inefficient. Biased estimation methods can address multicollinearity in data. This study proposes a Stein estimator, a biased estimation method, for the COMPRM that can simultaneously address correlated regressors and dispersion issues. The estimated mean square error (EMSE) is used to evaluate performance. The proposed estimator's performance is assessed both theoretically and numerically. The numerical evaluations include a simulation study under various parametric conditions and a real-world application. The results from both the simulation study and the real application demonstrate that the Stein estimator outperforms the MLE.

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### 1. Introduction

Count data models are widely used for counting responses. One of the most popular models is the Poisson model. The Poisson model works with a single parameter as the mean and variance are equal. This property reduces its application and is unable to explain the dispersion problem. Different models are proposed to handle dispersion. Examples include the negative binomial model (Hilbe, 2011), the bell regression model (Majid et al., 2022), and the Poisson mixture, which are used for over-dispersed data and cannot handle underdispersion cases (McLachlan, 1997). A Conway-Maxwell Poisson regression model (COMPRM) can capture both over and under-dispersion for modeling queuing systems with state-dependent service rates introduced by Conwaay and Maxwell (1962).

Moreover, the count data models may be with correlated regressors. In this situation, the maximum likelihood estimator (MLE) provides an inefficient regression coefficient estimate. To address the issue

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of correlated regressors, Stein proposed the Stein estimator (SE) for the LRM (Stein, 1960). Stein estimator is proposed for the logistic regression model. In his study, he presented three biased estimators, ridge, Stein, and principal component regression, and compared them using a Monte Carlo simulation study, but no theoretical comparison is provided (Schaefer, 1986). For the Inverse Gaussian Regression Model, SE performs as an efficient proposed estimator (Akram et al., 2021).

The SE for the logistic regression was proposed by Schaefer (1986). The SE for the Poisson regression model as a case of count data model deals with correlated regressors and equal dispersion by Amin et al. (2022). Akram et al. (2021) considered the SE for the inverse Gaussian regression model. Recently, the SE was adapted for the beta regression model (Amin et al., 2023a). The response variable might be in count form with overdispersion, underdispersion, and correlated regressors. Therefore, we need a biased estimator for the COMPRM. We are considering using the SE as a biased estimator to address the issue of correlated regressors in the COMPRM. Although some researchers have studied this biased estimator, there is no study specifically on using the SE for the COMPRM to address correlated regressors. Thus, we propose a new estimator, the COMP Stein Estimator (COMPSE), to reduce the impact of correlated regressors. The remainder of this study is organized

as follows: Section 2 introduces the COMPRM model and its estimation methods. Additionally, we explain COMPRM and COMPSE along with their MSEs and provide a theoretical comparison of the proposed estimator with the Maximum Likelihood Estimator (MLE). In Section 3, we assess the performance of the estimator using a Monte Carlo simulation. Section 4 involves the application of the model to real data. The final section summarizes the conclusions of the study.

### 2. Methodology

### 2.1. The COMP regression model

The COMP distribution is flexible enough to handle the dispersion in count data with an additional parameter ( $\nu$ ) and deals with both overdispersion ( $\nu < 1$ ) and under dispersion ( $\nu > 1$ ). The COMP distribution is the generalization of some well-known discrete distributions. When  $\nu =1$ , then the COMP distribution approaches the Poisson distribution, when  $\nu =0$  and  $\lambda < 1$ , the COMP distribution is converted to Geometric distribution, and when  $\nu \rightarrow \infty$ , the COMP distribution approaches the Bernoulli distribution with probability  $\left(\frac{\lambda}{1+\lambda}\right)$ . Suppose y is a random variable and follows a COMP ( $\lambda, \nu$ ) with a probability mass function as

$$P(Y = y; \lambda, \nu) = \frac{1}{Z(\lambda, \nu)} \frac{\lambda^{y}}{(y!)^{\nu'}} \quad y = 0, 1, 2, \dots, \infty$$
(1)

where,  $Z(\lambda, \nu) = \sum_{n=0}^{\infty} \frac{\lambda^n}{(n!)^{\nu}}$  is the normalizing constant,  $\lambda$  is the mean parameter, and  $\nu$  ( $\nu > 0$ ) is the dispersion parameter (Chatla and Shmueli, 2018). The mean and variance of the COMP distribution using an asymptotic expression for Z in Eq. 1 are, respectively (Shmueli et al., 2005).

$$E(Y) \approx \lambda^{\frac{1}{\nu}} + \frac{1}{2\nu} - \frac{1}{2'},$$
  

$$Var(Y) \approx \frac{1}{\nu} \lambda^{\frac{1}{\nu}}$$
(2)

The reparametrized COMP function is obtained by setting  $\mu = \lambda^{\frac{1}{\nu}}$  in Eq. 1 (Guikema and Goffelt, 2008). The new formulation of (1) is given as,

$$P(Y = y; \mu, \nu) = \frac{1}{S(\mu, \nu)} \left(\frac{\mu^{y}}{y!}\right)^{\nu}, \ y = 0, 1, 2, ..., \infty$$
(3)

where,

$$S(\mu,\nu) = \sum_{n=0}^{\infty} \left(\frac{\mu^n}{n!}\right)^{\nu} \tag{4}$$

The mean and variance of the distribution from Eq. 3 are derived as  $E(Y) \approx \mu + \frac{1}{2}\nu - \frac{1}{2}$  and  $Var(Y) \approx \frac{\mu}{\nu}$ , it becomes accurate for  $\mu > 10$  and  $\nu \leq 1$  (Shmueli et al., 2005). Now, the new parameterization allows  $\mu$  and  $\nu$  as centering and shape parameters, respectively. The COMPRM consists of two types of models: the mean model and the dispersion model.

The COMP regression model is a dual-link GLM, as mean and variance depend on covariates. Y is the count variable (response variable),  $x_i$  and  $z_i$  are the covariates used in the mean link function and variance link function with p and q terms, respectively (Francis et al., 2012).

$$ln(\mu_i) = \beta_0 + \sum_{j=1}^p \beta_j x_{ij} = x_i^t \beta$$
(5)

$$ln(v_i) = \delta_0 + \sum_{k=1}^q \delta_k z_{ik} = z_i^t \delta$$
(6)

The mean and variance models in Eqs. 5 and 6 are used to estimate the coefficients of the COMPRM. For simplicity, we will assume a single value of v and use the mean model for estimation purposes. Let  $\eta_i = log(\mu_i) = x'_i\beta$  is the linear predictor with a log link, where  $\beta$  is the vector of regression coefficients, including the intercept. Based on the new formulation, the likelihood function of Eq. 3 (Francis et al., 2012). The log-likelihood function can be written as

$$l(y_{i}; \beta, \nu) = \nu \sum_{i=1}^{n} y_{i} \eta_{i} - \sum_{i=1}^{n} \nu \log(y_{i}!) - \sum_{i=1}^{n} \log[S(\eta_{i}, \nu)]$$
(7)

For the estimation of parameters vector  $\beta$  and dispersion parameter v, we solve the log-likelihood function defined in Eq. 7. For this purpose, by differentiating Eq. 7 w.r.t  $\beta$  and  $\nu$ , it becomes (Francis et al., 2012).

$$\frac{\partial l}{\partial \beta_j} = \sum_{i=1}^n (y_i \nu - \frac{\partial}{\partial \eta_i} \log[S(\eta_i, \nu)]) x_{ij}$$
(8)

$$\frac{\partial l}{\partial \nu} = \sum_{i=1}^{n} (-\log(y_i!) - \frac{\partial}{\partial \nu} \log[S(\eta_i, \nu)])$$
(9)

The solution to Eqs. 8 and 9 is obtained using the iterative reweighted least squares (IRLS) method (Sellers and Shmueli, 2010). To estimate the parameter  $\beta$ , it is necessary to fix v, and the same procedure applies to estimate the second parameter. For more details, refer to Shmueli et al. (2005). One disadvantage of using the MLE is that the variance becomes inflated when there is severe collinearity among the explanatory variables. Under these conditions, it becomes very difficult to determine whether the regression coefficients are significant. Fixing v, the maximum likelihood (ML) of  $\beta$  is,

$$\hat{\beta}_{MLE} = (S)^{-1} X^t \widehat{W} q, \tag{10}$$

where,  $S = X^t \widehat{W}X$ ,  $q = log(\widehat{\mu}) + \frac{(y-\widehat{\mu})}{Var(\widehat{\mu})}$  is a vector of the adjusted response variable, and  $\widehat{W}$  is a matrix of weights, i.e.  $\widehat{W} = diag(V_i)$ , where  $V_i = \frac{\tau_i}{\nu} + \frac{v_i^2 - 1}{24v_i^3}\tau_i^{-1} + \frac{v_i^2 - 1}{12v_i^4}\tau_i^{-2} + \frac{v_i^2 - 1}{6v_i^5}\tau_i^{-3}$  with  $\tau_i = \frac{\widehat{\mu}_i}{\nu}$ .  $\widehat{V}$  and q both are evaluated by using the Fisher scoring procedure. The matrix MSE (MMSE) and scalar MSE of Eq. 10 are respectively given as,

$$MSE(\hat{\beta}_{MLE}) = E(\hat{\beta}_{MLE} - \beta)^{\iota}(\hat{\beta}_{MLE} - \beta)$$
$$MSE(\hat{\beta}_{MLE}) = \hat{v}tr(S) = \hat{v}\sum_{j=1}^{r} \frac{1}{\lambda_{i}'}$$
(11)

where,  $\lambda_j$  is the jth eigenvalue of the *S* matrix,  $\hat{\nu}$  is estimated dispersion parameter.

a.,

## 2.2. The Stein estimator for COMP regression model

Stein (1960) proposed an estimator as a remedy for correlated regressors in the LRM. For the COMPRM, we proposed a Stein estimator to overcome the effect of correlated regressors. The proposed COMPSE is defined as:

$$\hat{\beta}_s = c\hat{\beta}_{MLE},\tag{12}$$

where, c (0 < c < 1) is the Stein parameter. When c=1,  $\hat{\beta}_{COMPSE} = \hat{\beta}_{MLE}$ . The estimated bias and covariance of Eq. 12 can be computed as,

$$Bias(\hat{\beta}_s) = E(\hat{\beta}_s) - \beta$$
  

$$Bias(\hat{\beta}_s) = c\beta - \beta$$
  

$$Bias = Bias(\hat{\beta}_s) = (c - I_r)\beta,$$
(13)

where,  $I_r$  is the identity matrix of order  $r \times r$ . The variance of the COMPSE is calculated as,

$$Cov(\hat{\beta}_{s}) = c^{2}Cov(\hat{\beta}_{MLE})$$

$$MSE(\hat{\beta}_{s}) = Cov(\hat{\beta}_{s}) + Bias(\hat{\beta}_{s})^{2}$$

$$MSE(\hat{\beta}_{s}) = \hat{\nu}\sum_{j=1}^{r}\frac{c^{2}}{\lambda_{j}} + (c-1)^{2}\sum_{j=1}^{r}\alpha_{j}^{2},$$
(14)

where,  $\alpha_j^2$  is the jth element of  $Q^t \hat{\beta}_{MLE}$  and Q is the eigenvector of the matrix  $Q(\Lambda)Q^t$ , where  $\Lambda = diag(\lambda_j)$  and *c* is a biasing parameter of the COMPSE and  $\lambda_j$  are eigenvalues. The MSE of the COMPSE depends on the value of *c*. An appropriate value of the *c* yields the minimum MSE of the COMPSE. Therefore, we suggest some new estimating methods to estimate the value of *c* for the COMPSE in the next subsection.

### 2.3. Proposed biasing parameters

For the selection of the biasing parameter, an optimum value of the biasing parameter can be obtained by taking a derivative of Eq. 14 and equating it to zero,

$$\frac{\frac{\partial (MSE(\hat{\beta}_s))}{\partial c}}{\sum_{j=1}^{r} 2c(\hat{\nu} + \lambda_j \alpha_j^2)} = 2\sum_{j=1}^{r} \alpha_j^2 \lambda_j.$$

On simplification, we obtain the value of *c* as,

$$c = \frac{\sum_{j=1}^{r} \alpha_j^2 \lambda_j}{\sum_{j=1}^{r} \nu + \alpha_j^2 \lambda_j}.$$
(15)

Based on the work of Hoerl and Kennard (1970) and Kibria (2003), Eq. 15 generally can be written as

$$c_j = \frac{\alpha_j^2 \lambda_j}{\nu + \alpha_j^2 \lambda_j}$$

Furthermore, using the above expression, we proposed the following biasing parameters for the COMPSE,

$$c_1 = \max(c_j),\tag{16}$$

$$c_2 = \frac{\prod_{j=1}^r c_j^{(1/r)}}{\max(c_i)},\tag{17}$$

$$c_3 = \begin{pmatrix} 1 \\ - \end{pmatrix} \sum_{i=1}^r c_i, \tag{18}$$

$$c_4 = median(c_j), \tag{19}$$

$$c_5 = \prod_{j=1}^r c_j^{(1/r)}, \tag{20}$$

$$c_6 = \frac{\sum_{j=1}^{j} \alpha_j}{\sum_{j=1}^{r} \alpha_j^2 + \nu \sum_{j=1}^{r} \frac{1}{\lambda_j}}.$$
 (21)

### 2.4. The theoretical comparison of the proposed estimator

The superiority of the COMPSE is compared with the MLE using the following theorem.

**Lemma 2.1:** Let M be a positive definite (p.d.) matrix, a be a vector of nonzero constants and c be a positive constant. Then  $cM - \alpha \alpha^t > 0$  if and only if  $\alpha^t M \alpha < c$  (Farebrother, 1976).

**Theorem 2.1:** Under COMPSE, consider c > 0,  $b_{COMPSE} = Bias(\hat{\beta}_{COMPSE})$  is the bias of COMPSE then  $MSE(\hat{\beta}_{MLE}) - MSE(\hat{\beta}_{COMPSE}) > 0$  if  $b_{COMPSE}[\hat{v}(S)^{-1} - \hat{v}c^{2}((S)^{-1})] b_{COMPSE}^{t} < 1$ .

**Proof**: The difference in MSE from Eqs. 11 and 14 can be,

$$\Delta_1 = MMSE(\hat{\beta}_{MLE}) - MMSE(\hat{\beta}_{COMPSE})$$
  
=  $\hat{v}[(S)^{-1} - c^2((S)^{-1})] - b_{COMPSE}b_{COMPSE}^t.$  (22)

From Eq. 22, we can write it as,

 $= \hat{v}(S)^{-1}[1-c^2] - b_{COMPSE}b_{COMPSE}^t$ 

The difference between the scalar MSE functions of MLE and COMPSE is as,

$$\begin{split} & MSE(\hat{\beta}_{MLE}) - MSE(\hat{\beta}_{COMPSE}) \\ &= \sum_{j=1}^{r} \left( \frac{\hat{v}}{\lambda_j} - \frac{\hat{v}c^2}{\lambda_j} + (c-1)^2 \alpha_j^2 \right) \\ &= \sum_{j=1}^{r} \left( \hat{v} \frac{(1-c^2)}{\lambda_j} + (c-1)^2 \alpha_j^2 \right) \end{split}$$

On simplifying the results, we get

$$MSE(\hat{\beta}_{MLE}) - MSE(\hat{\beta}_{COMPSE}) = \hat{v} \sum_{j=1}^{r} \left( \frac{(1-c^2) + \lambda_j(c-1)^2 \alpha_j^2}{\lambda_j} \right).$$

The expression  $\hat{v}[(S)^{-1}c^2]$  is p.d if  $[1-c^2] > 0$ . Thus if 0 < c < 1, then the theorem is completed by Lemma 2.1 and it is enough to prove that the COMPSE is superior to the MLE in the form of scalar MSE for the COMPRM.

### 3. Monte Carlo simulation study

This section contains a numerical evaluation of the proposed estimator and a comparison with MLE using a Monte Carlo simulation. For this purpose, various factors are taken with different values. These factors include sample size, dispersion, correlated regressors, and the number of explanatory variables. The assumed values of these factors are given in Table 1.

 Table 1: Assumed values of different factors for simulation

stud	study						
Factors	Notation	Values					
Number of explanatory variables	р	3,6,9,12					
Number of replicates	R	1000					
Dispersion parameter	v	0.85,1,1.25					
Sample size	n	50,100,150,200					
Degree of correlation	$\rho^2$	0.8,0.9,0.95,0.99					

The response variable of the COMPRM is generated from a *CMP* ( $\mu_i$ ,  $\nu$ ) distribution, where:

$$\mu_{i} = exp(\beta_{0} + \beta_{1}x_{i1} + \dots + \beta_{p}x_{ip}), \quad i = 1, \dots, n.$$
(23)

The correlated explanatory variables are generated as follows (Kibria, 2003).

$$x_{ij} = (1 - \rho^2)^{1/2} z_{ij} + \rho z_{i(j+1)}, i = 1, \dots, n; j = 1, \dots, p.$$
 (24)

where,  $z_{ij}$  are the independent standard normal pseudo-random numbers. The regression parameters are selected in such a way that  $\sum_{j=1}^{p} \beta_j^2 = 1$ , which is a commonly used restriction in the field (Amin et al., 2023b). For the different combinations of  $n, p, \rho, v$ , the data is repeatedly generated 1000 times. The MSE criteria is used to gauge the performance of the estimators, which is defined by,

$$MSE(\hat{\beta}) = \frac{\sum_{i=1}^{R} (\hat{\beta}_i - \beta)^{i} (\hat{\beta}_i - \beta)}{R},$$
(25)

where,  $(\hat{\beta}_i - \beta)$  is the difference between the true parameter and estimated vectors of the proposed and other considered estimators at *i*th replication, and *R* represents the number of replications.

### 3.1. Results and discussions

The simulation study is performed under the various factors listed in Table 1. The estimated MSEs of the considered estimators are given in Tables 2-13. The summary of simulation results is as follows,

- Table 2 presents the estimated mean square error (EMSE) for p=3 and v=0.85 for the overdispersion case. It is observed that COMPSE with  $c_5$  at sample size n=50,100,150, and 200 has minimum EMSE for all levels of multicollinearity as compared to the MLE and COMPSE with all other proposed Stien parameter estimators.
- On comparing the results of the proposed estimator concerning sample size, it is observed that an increase in sample size causes a decrease in the values of EMSEs. From Table 2, it is observed that for a fixed level of multicollinearity 0.80, *p*=3, and *v*=0.85, the EMSEs are 0.8777, 0.8440, 0.8835, and 0.8484, respectively. Hence, the gradual decrease in values of EMSEs shows the efficiency of the proposed estimator to combat multicollinearity by increasing the sample size.
- From Table 3, for all levels of multicollinearity, when p=3, v=1, and n=50, the values of EMSEs of  $c_5$  are 0.9797, 1.6971, 1.8197 and 5.8784. So, the performance as a function of multicollinearity for the fixed *n*, *p*, and *v* shows an increasing trend as

the level of multicollinearity increases for the EMSE of the COMPSE. The same pattern is observed in Tables 2-13.

• Tables 2, 5, 8, and 11 present the EMSE for p=3, 6, 9, and 12, respectively, showing that as the number of explanatory variables increases, the EMSEs of the estimators also increase. For p=3, Tables 2, 3, and 4 represent the estimated MSE for overdispersion, equidispersion, and underdispersion, respectively. The results clearly show that the EMSE is the least affected by overdispersion as compared to the equal and under-dispersion cases.

#### 4. Application: Plastic plywood data

In this section, the performance of the proposed estimator is evaluated with the help of a real-life dataset that is related to the plastic plywood dataset. This application was considered by many researchers with different variables (Azaman et al., 2013; Demirkir et al., 2013; Fang et al., 2014). We consider this application to evaluate the performance of our proposed method and compare it with the MLE. This application consists of n=100observations, where the response variable y represents the number of defects that may increase or decrease per laminated plastic plywood area. The four explanatory variables include volumetric shrinkage  $(x_1)$ , assembly time  $(x_2)$ , wood density  $(x_3)$  and drying temperature  $(x_4)$ .

The estimated dispersion parameter is found to be  $\hat{v} = 0.9614$ , which indicates that there is overdispersion in the data set. In the regression model, commonly used methods are variance inflation factor (VIF) and condition index (CI) to test multicollinearity among the explanatory the variables. The  $CI = \sqrt{\lambda_{max}/\lambda_{min}} = 8634.73$  of this data set shows severe multicollinearity among the explanatory variables. Hence, we use the COMPSE to overcome the effect of correlated explanatory variables in the COMPRM. The MSEs of the MLE and COMPSE with different shrinkage parameters are computed using Eqs. 11 and 14, respectively. The estimated regression coefficients and MSEs of different shrinkage parameters of the MLE, COMPSE are mentioned in Table 14. On comparing the performance of the COMPRM estimators, it is observed that our newly proposed estimator (COMPSE) with all five Stein parameters outperforms as compared to the MLE. Furthermore, when there are highly correlated regressors, MLE is the estimator that is most negatively affected.

#### 5. Conclusion

In this study, we introduced a new estimator, the COMPSE, for the COMPRM to reduce the impact of correlated regressors. We evaluated the proposed estimator using a Monte Carlo simulation study, with the EMSE as the performance criterion, where a lower EMSE indicates better performance.

**Table 2:** EMSEs for v = 0.85 and p=3

					COMPSE			
n	$\rho^2$	MLE						
50	0.0		<i>C</i> <sub>1</sub>	C <sub>2</sub>	<i>C</i> <sub>3</sub>	C <sub>4</sub>	<i>c</i> <sub>5</sub>	C <sub>6</sub>
50	0.8	1.8731	1.8540	0.8804	0.8810	1.0033	0.8777	1.0032
	0.9	3.7777	3.7405	1.3522	1.6757	1.9509	1.3453	1.9268
	0.95	6.3936	6.3326	2.1981	2.9232	3.5155	2.1831	2.9709
	0.99	36.5167	36.248	9.7654	16.282	20.312	9.6973	14.9107
100	0.8	1.6016	1.5950	0.8449	0.8377	0.9673	0.8440	0.9471
100			1.3930			0.9073		
	0.9	3.2445	3.2312	1.2556	1.5366	1.8255	1.2531	1.7311
	0.95	5.9275	5.9035	1.9772	2.7852	3.4530	1.9718	2.9880
	0.99	30.8726	30.7512	9.1390	15.311	19.717	9.1046	14.0608
150	0.8	1.7464	1.7419	0.8842	0.9127	1.0502	0.8835	1.0923
150				1 2421	1 4 - 1 1	1.7099		1.6625
	0.9	2.8779	2.8707	1.2421	1.4511	1.7099	1.2405	
	0.95	5.6424	5.6276	1.9006	2.7152	3.4022	1.8974	3.0410
	0.99	24.2021	24.1431	6.2130	11.498	15.362	6.1995	10.9629
200	0.8	1.6339	1.6308	0.8488	0.8685	0.9873	0.8484	1.0202
	0.9	3.1381	3.1319	1.2212	1.5147	1.8416	1.2200	1.7888
	0.95	5.7624			2.8449	3.4706		3.0242
			5.7516	2.0636	2.0449		2.0610	
	0.99	20.2210	18.2341	5.1223	10.2120	14.7563	5.0100	10.1180
			Bol	d indicated the sma	aller EMSE			
			Table 3	<b>B:</b> EMSEs for $\nu$				
n	$ ho^2$	MLE	<i>C</i> <sub>1</sub>	<i>C</i> <sub>2</sub>	COMPSE c <sub>3</sub>	<i>C</i> <sub>4</sub>	C <sub>5</sub>	<i>c</i> <sub>6</sub>
50	0.8	2.5216	2.4943	0.9838	1.0589	1.1279	0.9797	1.2586
50		4 2002				1.14/7	1 (074	
	0.9	4.3082	4.2689	1.7066	2.0857	2.4095	1.6971	2.3400
	0.95	6.1630	6.1047	1.8304	2.6973	3.3640	1.8197	2.7369
	0.99	32.3845	32.1564	5.9207	13.202	17.2830	5.8784	12.9325
100	0.8	1.5628	1.5558	0.8833	0.8280	0.9490	0.8823	0.9180
	0.9	3.6075	3.5937	1.4076	1.7506	2.0526	1.4047	2.0296
	0.7					2.0320	1.404/	
	0.95	6.3364	6.3088	1.9269	2.8399	3.5250	1.9215	2.9814
	0.99	31.6043	31.4819	8.6775	15.6335	20.8690	8.6456	14.6645
150	0.8	1.5385	1.5344	0.8700	0.8412	0.9892	0.8695	0.9504
	0.9	3.0156	3.0077	1.0583	1.3934	1.7623	1.0572	1.6466
	0.95	5.9811	5.9659	2.2116	3.0050	3.7501	2.2077	3.1833
	0.95							
	0.99	30.9721	30.8964	8.5471	15.0428	19.7190	8.5288	15.1740
200	0.8	1.7666	1.7632	0.9769	0.9950	1.1539	0.9762	1.1245
	0.9	3.0860	3.0800	1.1884	1.5256	1.9210	1.1873	1.7502
	0.95	5.2988	5.2891	2.0396	2.7508	3.3882	2.0371	2.9301
	0.99	26.1379	26.0902	7.3227	12.9054	17.1422	7.3106	12.8037
	0.99	20.1379		d indicated the sma		17.1422	7.3100	12.0037
			Table 4:	EMSEs for $\nu =$	= 1.25 and <i>p</i> =3 COMPSE			
n	ρ <sup>2</sup> —	MLE	<i>C</i> <sub>1</sub>	<i>c</i> <sub>2</sub>	COMF3E C3	<i>C</i> <sub>4</sub>	<i>C</i> <sub>5</sub>	<i>C</i> <sub>6</sub>
<b>T</b> 0			3.5115	1.1557	1.3714	1.5082	1.1383	1.3434
50	0.8	3.6527						110 10 1
50	0.8	3.6527						2 4700
50	0.9	8.3539	8.0320	1.7971	2.7803	2.9743	1.7514	2.4708
50	0.9 0.95	8.3539 15.0446	8.0320 14.4979	1.7971 3.6317	2.7803 5.6743	2.9743 6.4204	1.7514 3.5207	4.3157
50	0.9	8.3539	8.0320	1.7971	2.7803	2.9743 6.4204 38.3932	1.7514	2.4708 4.3157 22.5578
	0.9 0.95 0.99	8.3539 15.0446 82.8496	8.0320 14.4979 81.0760	1.7971 3.6317 18.7003	2.7803 5.6743 32.9074	2.9743 6.4204 38.3932	1.7514 3.5207 18.2613	4.3157 22.5578
	0.9 0.95 0.99 0.8	8.3539 15.0446 82.8496 3.9743	8.0320 14.4979 81.0760 3.9003	1.7971 3.6317 18.7003 1.2142	2.7803 5.6743 32.9074 1.5167	2.9743 6.4204 38.3932 1.6707	1.7514 3.5207 18.2613 1.2051	4.3157 22.5578 1.6109
	0.9 0.95 0.99 0.8 0.9	8.3539 15.0446 82.8496 3.9743 6.6259	8.0320 14.4979 81.0760 3.9003 6.5054	1.7971 3.6317 18.7003 1.2142 1.4900	2.7803 5.6743 32.9074 1.5167 2.4166	2.9743 6.4204 38.3932 1.6707 2.7908	1.7514 3.5207 18.2613 1.2051 1.4765	4.3157 22.5578 1.6109 2.2696
	0.9 0.95 0.99 0.8 0.9 0.95	8.3539 15.0446 82.8496 3.9743 6.6259 13.4735	8.0320 14.4979 81.0760 3.9003 6.5054 13.2394	1.7971 3.6317 18.7003 1.2142 1.4900 2.7931	2.7803 5.6743 32.9074 1.5167 2.4166 5.1436	2.9743 6.4204 38.3932 1.6707 2.7908 6.1981	1.7514 3.5207 18.2613 1.2051 1.4765 2.7563	4.3157 22.5578 1.6109 2.2696 3.9640
100	0.9 0.95 0.99 0.8 0.9 0.95 0.99	8.3539 15.0446 82.8496 3.9743 6.6259 13.4735 69.8082	8.0320 14.4979 81.0760 3.9003 6.5054 13.2394 68.7806	1.7971 3.6317 18.7003 1.2142 1.4900 2.7931 10.9614	2.7803 5.6743 32.9074 1.5167 2.4166 5.1436 28.0143	2.9743 6.4204 38.3932 1.6707 2.7908 6.1981 36.7776	1.7514 3.5207 18.2613 1.2051 1.4765 2.7563 10.7996	4.3157 22.5578 1.6109 2.2696 3.9640 19.0875
100	0.9 0.95 0.99 0.8 0.9 0.95	8.3539 15.0446 82.8496 3.9743 6.6259 13.4735	8.0320 14.4979 81.0760 3.9003 6.5054 13.2394	1.7971 3.6317 18.7003 1.2142 1.4900 2.7931	2.7803 5.6743 32.9074 1.5167 2.4166 5.1436	2.9743 6.4204 38.3932 1.6707 2.7908 6.1981	1.7514 3.5207 18.2613 1.2051 1.4765 2.7563	4.3157 22.5578 1.6109 2.2696 3.9640
100	0.9 0.95 0.99 0.8 0.9 0.95 0.99 0.8	8.3539 15.0446 82.8496 3.9743 6.6259 13.4735 69.8082 3.7132	8.0320 14.4979 81.0760 3.9003 6.5054 13.2394 68.7806 3.6685	1.7971 3.6317 18.7003 1.2142 1.4900 2.7931 10.9614 1.1713	2.7803 5.6743 32.9074 1.5167 2.4166 5.1436 28.0143 1.4597	2.9743 6.4204 38.3932 1.6707 2.7908 6.1981 36.7776 1.6050	1.7514 3.5207 18.2613 1.2051 1.4765 2.7563 10.7996 1.1657	4.3157 22.5578 1.6109 2.2696 3.9640 19.0875 1.5676
100	0.9 0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.99 0.8 0.9	8.3539 15.0446 82.8496 3.9743 6.6259 13.4735 69.8082 3.7132 5.7822	8.0320 14.4979 81.0760 3.9003 6.5054 13.2394 68.7806 3.6685 5.7136	$\begin{array}{c} 1.7971\\ 3.6317\\ 18.7003\\ 1.2142\\ 1.4900\\ 2.7931\\ 10.9614\\ 1.1713\\ 1.4829\end{array}$	2.7803 5.6743 32.9074 1.5167 2.4166 5.1436 28.0143 1.4597 2.0971	2.9743 6.4204 38.3932 1.6707 2.7908 6.1981 36.7776 1.6050 2.3049	1.7514 3.5207 18.2613 1.2051 1.4765 2.7563 10.7996 1.1657 1.4741	4.3157 22.5578 1.6109 2.2696 3.9640 19.0875 1.5676 1.9301
100	0.9 0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.9 0.8 0.9	8.3539 15.0446 82.8496 3.9743 6.6259 13.4735 69.8082 3.7132 5.7822 11.4546	8.0320 14.4979 81.0760 3.9003 6.5054 13.2394 68.7806 3.6685 5.7136 11.3204	$\begin{array}{c} 1.7971\\ 3.6317\\ 18.7003\\ 1.2142\\ 1.4900\\ 2.7931\\ 10.9614\\ 1.1713\\ 1.4829\\ 2.2450\\ \end{array}$	2.7803 5.6743 32.9074 1.5167 2.4166 5.1436 28.0143 1.4597 2.0971 4.2160	2.9743 6.4204 38.3932 1.6707 2.7908 6.1981 36.7776 1.6050 2.3049 5.0250	1.7514 3.5207 18.2613 1.2051 1.4765 2.7563 10.7996 1.1657 1.4741 2.2270	4.3157 22.5578 1.6109 2.2696 3.9640 19.0875 1.5676 1.9301 3.3182
100 150	0.9 0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.9 0.8 0.9 0.95 0.99	8.3539 15.0446 82.8496 3.9743 6.6259 13.4735 69.8082 3.7132 5.7822 11.4546 65.2814	8.0320 14.4979 81.0760 3.9003 6.5054 13.2394 68.7806 3.6685 5.7136 11.3204 64.6202	$\begin{array}{c} 1.7971\\ 3.6317\\ 18.7003\\ 1.2142\\ 1.4900\\ 2.7931\\ 10.9614\\ 1.1713\\ 1.4829\\ 2.2450\\ 11.0595 \end{array}$	2.7803 5.6743 32.9074 1.5167 2.4166 5.1436 28.0143 1.4597 2.0971 4.2160 25.9822	$\begin{array}{c} 2.9743 \\ 6.4204 \\ 38.3932 \\ 1.6707 \\ 2.7908 \\ 6.1981 \\ 36.7776 \\ 1.6050 \\ 2.3049 \\ 5.0250 \\ 33.6440 \end{array}$	1.7514 3.5207 18.2613 1.2051 1.4765 2.7563 10.7996 1.1657 1.4741 2.2270 10.9467	4.3157 22.5578 1.6109 2.2696 3.9640 19.0875 1.5676 1.9301 3.3182 19.6371
100 150	0.9 0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.9 0.95 0.99 0.95 0.99 0.8	8.3539 15.0446 82.8496 3.9743 6.6259 13.4735 69.8082 3.7132 5.7822 11.4546 65.2814 3.5341	8.0320 14.4979 81.0760 3.9003 6.5054 13.2394 68.7806 3.6685 5.7136 11.3204 64.6202 3.5035	$\begin{array}{c} 1.7971\\ 3.6317\\ 18.7003\\ 1.2142\\ 1.4900\\ 2.7931\\ 10.9614\\ 1.1713\\ 1.4829\\ 2.2450\\ 11.0595\\ 1.2603\\ \end{array}$	2.7803 5.6743 32.9074 1.5167 2.4166 5.1436 28.0143 1.4597 2.0971 4.2160 25.9822 1.4582	$\begin{array}{c} 2.9743 \\ 6.4204 \\ 38.3932 \\ 1.6707 \\ 2.7908 \\ 6.1981 \\ 36.7776 \\ 1.6050 \\ 2.3049 \\ 5.0250 \\ 33.6440 \\ 1.5572 \end{array}$	1.7514 3.5207 18.2613 1.2051 1.4765 2.7563 10.7996 1.1657 1.4741 2.2270 10.9467 1.2555	4.3157 22.5578 1.6109 2.2696 3.9640 19.0875 1.5676 1.9301 3.3182 19.6371 1.5249
100 150	0.9 0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.9 0.8 0.9 0.95 0.99	8.3539 15.0446 82.8496 3.9743 6.6259 13.4735 69.8082 3.7132 5.7822 11.4546 65.2814	8.0320 14.4979 81.0760 3.9003 6.5054 13.2394 68.7806 3.6685 5.7136 11.3204 64.6202	$\begin{array}{c} 1.7971\\ 3.6317\\ 18.7003\\ 1.2142\\ 1.4900\\ 2.7931\\ 10.9614\\ 1.1713\\ 1.4829\\ 2.2450\\ 11.0595 \end{array}$	2.7803 5.6743 32.9074 1.5167 2.4166 5.1436 28.0143 1.4597 2.0971 4.2160 25.9822	$\begin{array}{c} 2.9743 \\ 6.4204 \\ 38.3932 \\ 1.6707 \\ 2.7908 \\ 6.1981 \\ 36.7776 \\ 1.6050 \\ 2.3049 \\ 5.0250 \\ 33.6440 \end{array}$	1.7514 3.5207 18.2613 1.2051 1.4765 2.7563 10.7996 1.1657 1.4741 2.2270 10.9467 1.2555 1.6952	4.3157 22.5578 1.6109 2.2696 3.9640 19.0875 1.5676 1.9301 3.3182 19.6371
100 150	0.9 0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.9 0.8 0.9	8.3539 15.0446 82.8496 3.9743 6.6259 13.4735 69.8082 3.7132 5.7822 11.4546 65.2814 3.5341 6.0415	8.0320 14.4979 81.0760 3.9003 6.5054 13.2394 68.7806 3.6685 5.7136 11.3204 64.6202 3.5035 5.9888	1.7971 3.6317 18.7003 1.2142 1.4900 2.7931 10.9614 1.1713 1.4829 2.2450 11.0595 1.2603 1.7040	2.7803 5.6743 32.9074 1.5167 2.4166 5.1436 28.0143 1.4597 2.0971 4.2160 25.9822 1.4582 2.3597	$\begin{array}{c} 2.9743 \\ 6.4204 \\ 38.3932 \\ 1.6707 \\ 2.7908 \\ 6.1981 \\ 36.7776 \\ 1.6050 \\ 2.3049 \\ 5.0250 \\ 33.6440 \\ 1.5572 \\ 2.6470 \end{array}$	1.7514 3.5207 18.2613 1.2051 1.4765 2.7563 10.7996 1.1657 1.4741 2.2270 10.9467 1.2555 1.6952	4.3157 22.5578 1.6109 2.2696 3.9640 19.0875 1.5676 1.9301 3.3182 19.6371 1.5249 1.9957
100 150	0.9 0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.9 0.8 0.9 0.9 0.9	8.3539 15.0446 82.8496 3.9743 6.6259 13.4735 69.8082 3.7132 5.7822 11.4546 65.2814 3.5341 6.0415 11.8783	8.0320 14.4979 81.0760 3.9003 6.5054 13.2394 68.7806 3.6685 5.7136 11.3204 64.6202 3.5035 5.9888 11.7739	1.7971 3.6317 18.7003 1.2142 1.4900 2.7931 10.9614 1.1713 1.4829 2.2450 11.0595 1.2603 1.7040 2.8339	2.7803 5.6743 32.9074 1.5167 2.4166 5.1436 28.0143 1.4597 2.0971 4.2160 25.9822 1.4582 2.3597 4.8364	2.9743 6.4204 38.3932 1.6707 2.7908 6.1981 36.7776 1.6050 2.3049 5.0250 33.6440 1.5572 2.6470 5.9326	1.7514 3.5207 18.2613 1.2051 1.4765 2.7563 10.7996 1.1657 1.4741 2.2270 10.9467 1.2555 1.6952 2.8151	4.3157 22.5578 1.6109 2.2696 3.9640 19.0875 1.5676 1.9301 3.3182 19.6371 1.5249 1.9957 4.0940
100 150	0.9 0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.99 0.8 0.9	8.3539 15.0446 82.8496 3.9743 6.6259 13.4735 69.8082 3.7132 5.7822 11.4546 65.2814 3.5341 6.0415	8.0320 14.4979 81.0760 3.9003 6.5054 13.2394 68.7806 3.6685 5.7136 11.3204 64.6202 3.5035 5.9888 11.7739 61.4578	1.7971 3.6317 18.7003 1.2142 1.4900 2.7931 10.9614 1.1713 1.4829 2.2450 11.0595 1.2603 1.7040	2.7803 5.6743 32.9074 1.5167 2.4166 5.1436 28.0143 1.4597 2.0971 4.2160 25.9822 1.4582 2.3597 4.8364 27.4905	$\begin{array}{c} 2.9743 \\ 6.4204 \\ 38.3932 \\ 1.6707 \\ 2.7908 \\ 6.1981 \\ 36.7776 \\ 1.6050 \\ 2.3049 \\ 5.0250 \\ 33.6440 \\ 1.5572 \\ 2.6470 \end{array}$	1.7514 3.5207 18.2613 1.2051 1.4765 2.7563 10.7996 1.1657 1.4741 2.2270 10.9467 1.2555 1.6952	4.3157 22.5578 1.6109 2.2696 3.9640 19.0875 1.5676 1.9301 3.3182 19.6371 1.5249 1.9957
100 150	0.9 0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.9 0.8 0.9 0.9 0.9	8.3539 15.0446 82.8496 3.9743 6.6259 13.4735 69.8082 3.7132 5.7822 11.4546 65.2814 3.5341 6.0415 11.8783	8.0320 14.4979 81.0760 3.9003 6.5054 13.2394 68.7806 3.6685 5.7136 11.3204 64.6202 3.5035 5.9888 11.7739 61.4578 Bol	1.7971 3.6317 18.7003 1.2142 1.4900 2.7931 10.9614 1.1713 1.4829 2.2450 11.0595 1.2603 1.7040 2.8339 <u>15.6510</u> d indicated the sma	2.7803 5.6743 32.9074 1.5167 2.4166 5.1436 28.0143 1.4597 2.0971 4.2160 25.9822 1.4582 2.3597 4.8364 27.4905 aller EMSE	2.9743 6.4204 38.3932 1.6707 2.7908 6.1981 36.7776 1.6050 2.3049 5.0250 33.6440 1.5572 2.6470 5.9326	1.7514 3.5207 18.2613 1.2051 1.4765 2.7563 10.7996 1.1657 1.4741 2.2270 10.9467 1.2555 1.6952 2.8151	4.3157 22.5578 1.6109 2.2696 3.9640 19.0875 1.5676 1.9301 3.3182 19.6371 1.5249 1.9957 4.0940
100 150 200	0.9 0.95 0.99 0.8 0.95 0.99 0.8 0.99 0.8 0.9 0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.9 0.95 0.99	8.3539 15.0446 82.8496 3.9743 6.6259 13.4735 69.8082 3.7132 5.7822 11.4546 65.2814 3.5341 6.0415 11.8783	8.0320 14.4979 81.0760 3.9003 6.5054 13.2394 68.7806 3.6685 5.7136 11.3204 64.6202 3.5035 5.9888 11.7739 61.4578 Bol	1.7971 3.6317 18.7003 1.2142 1.4900 2.7931 10.9614 1.1713 1.4829 2.2450 11.0595 1.2603 1.7040 2.8339 <u>15.6510</u> d indicated the small	2.7803 5.6743 32.9074 1.5167 2.4166 5.1436 28.0143 1.4597 2.0971 4.2160 25.9822 1.4582 2.3597 4.8364 27.4905 aller EMSE	2.9743 6.4204 38.3932 1.6707 2.7908 6.1981 36.7776 1.6050 2.3049 5.0250 33.6440 1.5572 2.6470 5.9326	1.7514 3.5207 18.2613 1.2051 1.4765 2.7563 10.7996 1.1657 1.4741 2.2270 10.9467 1.2555 1.6952 2.8151	4.3157 22.5578 1.6109 2.2696 3.9640 19.0875 1.5676 1.9301 3.3182 19.6371 1.5249 1.9957 4.0940
100 150 200 <i>n</i>	$\begin{array}{c} 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ \hline \end{array}$	8.3539 15.0446 82.8496 3.9743 6.6259 13.4735 69.8082 3.7132 5.7822 11.4546 65.2814 3.5341 6.0415 11.8783 61.9594 MLE	8.0320 14.4979 81.0760 3.9003 6.5054 13.2394 68.7806 3.6685 5.7136 11.3204 64.6202 3.5035 5.9888 11.7739 61.4578 Bol <b>Table 5:</b>	1.7971 3.6317 18.7003 1.2142 1.4900 2.7931 10.9614 1.1713 1.4829 2.2450 11.0595 1.2603 1.7040 2.8339 15.6510 d indicated the smatrix EMSEs for $\nu =$	2.7803 5.6743 32.9074 1.5167 2.4166 5.1436 28.0143 1.4597 2.0971 4.2160 25.9822 1.4582 2.3597 4.8364 27.4905 aller EMSE <b>compse</b> $c_3$	$\begin{array}{c} 2.9743\\ 6.4204\\ 38.3932\\ 1.6707\\ 2.7908\\ 6.1981\\ 36.7776\\ 1.6050\\ 2.3049\\ 5.0250\\ 33.6440\\ 1.5572\\ 2.6470\\ 5.9326\\ 34.2896\\ \end{array}$	$\begin{array}{c} 1.7514\\ 3.5207\\ 18.2613\\ 1.2051\\ 1.4765\\ 2.7563\\ 10.7996\\ 1.1657\\ 1.4741\\ 2.2270\\ 10.9467\\ 1.2555\\ 1.6952\\ 2.8151\\ 15.5287\\ \end{array}$	4.3157 22.5578 1.6109 2.2696 3.9640 19.0875 1.5676 1.9301 3.3182 19.6371 1.5249 1.9957 4.0940 18.7061
100 150 200	$\begin{array}{c} 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ \hline \end{array}$	8.3539 15.0446 82.8496 3.9743 6.6259 13.4735 69.8082 3.7132 5.7822 11.4546 65.2814 3.5341 6.0415 11.8783 61.9594 MLE 5.5244	8.0320 14.4979 81.0760 3.9003 6.5054 13.2394 68.7806 3.6685 5.7136 11.3204 64.6202 3.5035 5.9888 11.7739 61.4578 Bolt <b>Table 5:</b> 5.4716	$\begin{array}{c} 1.7971\\ 3.6317\\ 18.7003\\ 1.2142\\ 1.4900\\ 2.7931\\ 10.9614\\ 1.1713\\ 1.4829\\ 2.2450\\ 11.0595\\ 1.2603\\ 1.7040\\ 2.8339\\ 15.6510\\ d \text{ indicated the smaller}\\ EMSEs for $\nu= \\ \hline \hline \hline \hline \\ c_2\\ \hline 1.3559 \end{array}$	2.7803 5.6743 32.9074 1.5167 2.4166 5.1436 28.0143 1.4597 2.0971 4.2160 25.9822 1.4582 2.3597 4.8364 27.4905 aller EMSE <u>0.85 and p=6</u> <u>COMPSE</u> <u>c<sub>3</sub></u> 1.8922	$\begin{array}{c} 2.9743\\ 6.4204\\ 38.3932\\ 1.6707\\ 2.7908\\ 6.1981\\ 36.7776\\ 1.6050\\ 2.3049\\ 5.0250\\ 33.6440\\ 1.5572\\ 2.6470\\ 5.9326\\ 34.2896\\ \hline \end{array}$	$\begin{array}{c} 1.7514\\ 3.5207\\ 18.2613\\ 1.2051\\ 1.4765\\ 2.7563\\ 10.7996\\ 1.1657\\ 1.4741\\ 2.2270\\ 10.9467\\ 1.2555\\ 1.6952\\ 2.8151\\ 15.5287\\ \hline \end{array}$	4.3157 22.5578 1.6109 2.2696 3.9640 19.0875 1.5676 1.9301 3.3182 19.6371 1.5249 1.9957 4.0940 18.7061
100 150 200 n	$\begin{array}{c} 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ \hline \end{array}$	8.3539 15.0446 82.8496 3.9743 6.6259 13.4735 69.8082 3.7132 5.7822 11.4546 65.2814 3.5341 6.0415 11.8783 61.9594 MLE	8.0320 14.4979 81.0760 3.9003 6.5054 13.2394 68.7806 3.6685 5.7136 11.3204 64.6202 3.5035 5.9888 11.7739 61.4578 Bol <b>Table 5:</b>	1.7971 3.6317 18.7003 1.2142 1.4900 2.7931 10.9614 1.1713 1.4829 2.2450 11.0595 1.2603 1.7040 2.8339 15.6510 d indicated the smatrix EMSEs for $\nu =$	2.7803 5.6743 32.9074 1.5167 2.4166 5.1436 28.0143 1.4597 2.0971 4.2160 25.9822 1.4582 2.3597 4.8364 27.4905 aller EMSE <b>compse</b> $c_3$	$\begin{array}{c} 2.9743\\ 6.4204\\ 38.3932\\ 1.6707\\ 2.7908\\ 6.1981\\ 36.7776\\ 1.6050\\ 2.3049\\ 5.0250\\ 33.6440\\ 1.5572\\ 2.6470\\ 5.9326\\ 34.2896\\ \end{array}$	$\begin{array}{c} 1.7514\\ 3.5207\\ 18.2613\\ 1.2051\\ 1.4765\\ 2.7563\\ 10.7996\\ 1.1657\\ 1.4741\\ 2.2270\\ 10.9467\\ 1.2555\\ 1.6952\\ 2.8151\\ 15.5287\\ \end{array}$	4.3157 22.5578 1.6109 2.2696 3.9640 19.0875 1.5676 1.9301 3.3182 19.6371 1.5249 1.9957 4.0940 18.7061
100 150 200 n	$\begin{array}{c} 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.95 \\ 0.99 \\ \hline \end{array}$	8.3539 15.0446 82.8496 3.9743 6.6259 13.4735 69.8082 3.7132 5.7822 11.4546 65.2814 3.5341 6.0415 11.8783 61.9594 MLE 5.5244 10.0862	8.0320 14.4979 81.0760 3.9003 6.5054 13.2394 68.7806 3.6685 5.7136 11.3204 64.6202 3.5035 5.9888 11.7739 61.4578 Bolt <b>Table 5:</b> 5.4716 9.9881	1.7971 3.6317 18.7003 1.2142 1.4900 2.7931 10.9614 1.1713 1.4829 2.2450 11.0595 1.2603 1.7040 2.8339 15.6510 d indicated the smale EMSEs for $\nu = \frac{c_2}{1.3559}$ 1.7698	2.7803 5.6743 32.9074 1.5167 2.4166 5.1436 28.0143 1.4597 2.0971 4.2160 25.9822 1.4582 2.3597 4.8364 27.4905 aller EMSE compse $c_3$ 1.8922 3.0566	$\begin{array}{c} 2.9743\\ 6.4204\\ 38.3932\\ 1.6707\\ 2.7908\\ 6.1981\\ 36.7776\\ 1.6050\\ 2.3049\\ 5.0250\\ 33.6440\\ 1.5572\\ 2.6470\\ 5.9326\\ 34.2896\\ \hline \end{array}$	$\begin{array}{c} 1.7514\\ 3.5207\\ 18.2613\\ 1.2051\\ 1.4765\\ 2.7563\\ 10.7996\\ 1.1657\\ 1.4741\\ 2.2270\\ 10.9467\\ 1.2555\\ 1.6952\\ 2.8151\\ 15.5287\\ \hline \end{array}$	4.3157 22.5578 1.6109 2.2696 3.9640 19.0875 1.5676 1.9301 3.3182 19.6371 1.5249 1.9957 4.0940 18.7061
100 150 200 n	$\begin{array}{c} 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ \hline \\ \rho^2 \\ \hline \\ 0.8 \\ 0.9 \\ 0.95 \\ \hline \\ 0.9 \\ 0.95 \\ \hline \end{array}$	8.3539 15.0446 82.8496 3.9743 6.6259 13.4735 69.8082 3.7132 5.7822 11.4546 65.2814 3.5341 6.0415 11.8783 61.9594 MLE 5.5244 10.0862 21.7299	8.0320 14.4979 81.0760 3.9003 6.5054 13.2394 68.7806 3.6685 5.7136 11.3204 64.6202 3.5035 5.9888 11.7739 61.4578 Bol <b>Table 5:</b> 5.4716 9.9881 21.4923	1.7971 3.6317 18.7003 1.2142 1.4900 2.7931 10.9614 1.1713 1.4829 2.2450 11.0595 1.2603 1.7040 2.8339 15.6510 d indicated the sma EMSEs for $\nu = \frac{c_2}{1.3559}$ 1.7698 4.0275	2.7803 5.6743 32.9074 1.5167 2.4166 5.1436 28.0143 1.4597 2.0971 4.2160 25.9822 1.4582 2.3597 4.8364 27.4905 iller EMSE $c_3$ 1.8922 3.0566 7.2244	$\begin{array}{c} 2.9743\\ 6.4204\\ 38.3932\\ 1.6707\\ 2.7908\\ 6.1981\\ 36.7776\\ 1.6050\\ 2.3049\\ 5.0250\\ 33.6440\\ 1.5572\\ 2.6470\\ 5.9326\\ 34.2896\\ \hline \\ \hline \\ \hline \\ \hline \\ \hline \\ \hline \\ 2.0588\\ 3.3763\\ 8.3026\\ \end{array}$	$\begin{array}{c} 1.7514\\ 3.5207\\ 18.2613\\ 1.2051\\ 1.4765\\ 2.7563\\ 10.7996\\ 1.1657\\ 1.4741\\ 2.2270\\ 10.9467\\ 1.2555\\ 1.6952\\ 2.8151\\ 15.5287\\ \hline \end{array}$	4.3157 22.5578 1.6109 2.2696 3.9640 19.0875 1.5676 1.9301 3.3182 19.6371 1.5249 1.9957 4.0940 18.7061
100 150 200 <u>n</u> 50	$\begin{array}{c} 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.99 \\ 0.95 \\ 0.99 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ \hline \\ \rho^2 \\ \hline \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.95 \\ 0.99 \\ \hline \end{array}$	8.3539 15.0446 82.8496 3.9743 6.6259 13.4735 69.8082 3.7132 5.7822 11.4546 65.2814 3.5341 6.0415 11.8783 61.9594 MLE 5.5244 10.0862 21.7299 97.0780	8.0320 14.4979 81.0760 3.9003 6.5054 13.2394 68.7806 3.6685 5.7136 11.3204 64.6202 3.5035 5.9888 11.7739 61.4578 Bol <b>Table 5:</b> c <sub>1</sub> 5.4716 9.9881 21.4923 96.3202	1.7971 3.6317 18.7003 1.2142 1.4900 2.7931 10.9614 1.1713 1.4829 2.2450 11.0595 1.2603 1.7040 2.8339 15.6510 d indicated the smale EMSEs for $\nu = \frac{c_2}{1.3559}$ 1.7698 4.0275 12.2767	2.7803 5.6743 32.9074 1.5167 2.4166 5.1436 28.0143 1.4597 2.0971 4.2160 25.9822 1.4582 2.3597 4.8364 27.4905 aller EMSE $c_{3}$ 1.8922 3.0566 7.2244 28.0876	$\begin{array}{c} 2.9743\\ 6.4204\\ 38.3932\\ 1.6707\\ 2.7908\\ 6.1981\\ 36.7776\\ 1.6050\\ 2.3049\\ 5.0250\\ 33.6440\\ 1.5572\\ 2.6470\\ 5.9326\\ 34.2896\\ \hline \\ \hline$	$\begin{array}{c} 1.7514\\ 3.5207\\ 18.2613\\ 1.2051\\ 1.4765\\ 2.7563\\ 10.7996\\ 1.1657\\ 1.4741\\ 2.2270\\ 10.9467\\ 1.2555\\ 1.6952\\ 2.8151\\ 15.5287\\ \hline \\ \hline$	4.3157 22.5578 1.6109 2.2696 3.9640 19.0875 1.5676 1.9301 3.3182 19.6371 1.5249 1.9957 4.0940 18.7061
100 150 200 <u>n</u> 50	$\begin{array}{c} 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.95 \\ 0.99 \\ \hline \end{array}$	8.3539 15.0446 82.8496 3.9743 6.6259 13.4735 69.8082 3.7132 5.7822 11.4546 65.2814 3.5341 6.0415 11.8783 61.9594 MLE 5.5244 10.0862 21.7299 97.0780 4.4131	8.0320 14.4979 81.0760 3.9003 6.5054 13.2394 68.7806 3.6685 5.7136 11.3204 64.6202 3.5035 5.9888 11.7739 61.4578 Bol <b>Table 5:</b> <b>c</b> <sub>1</sub> 5.4716 9.9881 21.4923 96.3202 4.3941	1.7971 3.6317 18.7003 1.2142 1.4900 2.7931 10.9614 1.1713 1.4829 2.2450 11.0595 1.2603 1.7040 2.8339 15.6510 d indicated the smale EMSEs for $\nu = \frac{c_2}{1.3559}$ 1.7698 4.0275 12.2767 1.1299	2.7803 5.6743 32.9074 1.5167 2.4166 5.1436 28.0143 1.4597 2.0971 4.2160 25.9822 1.4582 2.3597 4.8364 27.4905 aller EMSE <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b> <b>c.3</b>	$\begin{array}{c} 2.9743\\ 6.4204\\ 38.3932\\ 1.6707\\ 2.7908\\ 6.1981\\ 36.7776\\ 1.6050\\ 2.3049\\ 5.0250\\ 33.6440\\ 1.5572\\ 2.6470\\ 5.9326\\ 34.2896\\ \hline \\ \hline$	$\begin{array}{c} 1.7514\\ 3.5207\\ 18.2613\\ 1.2051\\ 1.4765\\ 2.7563\\ 10.7996\\ 1.1657\\ 1.4741\\ 2.2270\\ 10.9467\\ 1.2555\\ 1.6952\\ 2.8151\\ 15.5287\\ \hline \\ \hline$	4.3157 22.5578 1.6109 2.2696 3.9640 19.0875 1.5676 1.9301 3.3182 19.6371 1.5249 1.9957 4.0940 18.7061
100 150 200 <u>n</u> 50	$\begin{array}{c} 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.95 \\ 0.99 \\ 0.95 \\ 0.99 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ \hline \end{array}$	8.3539 15.0446 82.8496 3.9743 6.6259 13.4735 69.8082 3.7132 5.7822 11.4546 65.2814 3.5341 6.0415 11.8783 61.9594 MLE 5.5244 10.0862 21.7299 97.0780	8.0320 14.4979 81.0760 3.9003 6.5054 13.2394 68.7806 3.6685 5.7136 11.3204 64.6202 3.5035 5.9888 11.7739 61.4578 Bol. <b>Table 5:</b> <b>C</b> 1 5.4716 9.9881 21.4923 96.3202 4.3941 7.9648	1.7971 3.6317 18.7003 1.2142 1.4900 2.7931 10.9614 1.1713 1.4829 2.2450 11.0595 1.2603 1.7040 2.8339 15.6510 d indicated the smale EMSEs for $\nu = \frac{c_2}{1.3559}$ 1.7698 4.0275 12.2767	2.7803 5.6743 32.9074 1.5167 2.4166 5.1436 28.0143 1.4597 2.0971 4.2160 25.9822 1.4582 2.3597 4.8364 27.4905 aller EMSE $c_{3}$ 1.8922 3.0566 7.2244 28.0876	$\begin{array}{c} 2.9743\\ 6.4204\\ 38.3932\\ 1.6707\\ 2.7908\\ 6.1981\\ 36.7776\\ 1.6050\\ 2.3049\\ 5.0250\\ 33.6440\\ 1.5572\\ 2.6470\\ 5.9326\\ 34.2896\\ \hline \\ \hline$	$\begin{array}{c} 1.7514\\ 3.5207\\ 18.2613\\ 1.2051\\ 1.4765\\ 2.7563\\ 10.7996\\ 1.1657\\ 1.4741\\ 2.2270\\ 10.9467\\ 1.2555\\ 1.6952\\ 2.8151\\ 15.5287\\ \hline \\ \hline$	4.3157 22.5578 1.6109 2.2696 3.9640 19.0875 1.5676 1.9301 3.3182 19.6371 1.5249 1.9957 4.0940 18.7061
100 150 200 <u>n</u> 50	$\begin{array}{c} 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ \hline \\ \rho^2 \\ \hline \\ \hline \\ \rho^2 \\ \hline \\ \hline \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.9 \\ 0.8 \\ 0.9$	8.3539 15.0446 82.8496 3.9743 6.6259 13.4735 69.8082 3.7132 5.7822 11.4546 65.2814 3.5341 6.0415 11.8783 61.9594 MLE 5.5244 10.0862 21.7299 97.0780 4.4131 8.0001	8.0320 14.4979 81.0760 3.9003 6.5054 13.2394 68.7806 3.6685 5.7136 11.3204 64.6202 3.5035 5.9888 11.7739 61.4578 Bol. <b>Table 5:</b> <b>C</b> 1 5.4716 9.9881 21.4923 96.3202 4.3941 7.9648	1.7971 3.6317 18.7003 1.2142 1.4900 2.7931 10.9614 1.1713 1.4829 2.2450 11.0595 1.2603 1.7040 2.8339 15.6510 d indicated the smather t	2.7803 5.6743 32.9074 1.5167 2.4166 5.1436 28.0143 1.4597 2.0971 4.2160 25.9822 1.4582 2.3597 4.8364 27.4905 aller EMSE <b>COMPSE</b> <b>c</b> <sub>3</sub> <b>1.8922</b> 3.0566 7.2244 28.0876 1.5226 2.66216	$\begin{array}{c} 2.9743\\ 6.4204\\ 38.3932\\ 1.6707\\ 2.7908\\ 6.1981\\ 36.7776\\ 1.6050\\ 2.3049\\ 5.0250\\ 33.6440\\ 1.5572\\ 2.6470\\ 5.9326\\ 34.2896\\ \hline \\ \hline$	$     \begin{array}{r}       1.7514 \\       3.5207 \\       18.2613 \\       1.2051 \\       1.4765 \\       2.7563 \\       10.7996 \\       1.1657 \\       1.4741 \\       2.2270 \\       10.9467 \\       1.2555 \\       1.6952 \\       2.8151 \\       15.5287 \\       \hline       \hline                     $	4.3157 22.5578 1.6109 2.2696 3.9640 19.0875 1.5676 1.9301 3.3182 19.6371 1.5249 1.9957 4.0940 18.7061
100 150 200 <u>n</u> 50	$\begin{array}{c} 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.95 \\ 0.99 \\ \hline \\ \rho^2 \\ \hline \\ \rho^2 \\ \hline \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.95 \\ \hline \end{array}$	8.3539 15.0446 82.8496 3.9743 6.6259 13.4735 69.8082 3.7132 5.7822 11.4546 65.2814 3.5341 6.0415 11.8783 61.9594 MLE 5.5244 10.0862 21.7299 97.0780 4.4131 8.0001 13.8590	8.0320 14.4979 81.0760 3.9003 6.5054 13.2394 68.7806 3.6685 5.7136 11.3204 64.6202 3.5035 5.9888 11.7739 61.4578 Bol. <b>Table 5:</b> <b>C</b> 1 5.4716 9.9881 21.4923 96.3202 4.3941 7.9648 13.7984	1.7971 3.6317 18.7003 1.2142 1.4900 2.7931 10.9614 1.1713 1.4829 2.2450 11.0595 1.2603 1.7040 2.8339 15.6510 d indicated the smather t	2.7803 5.6743 32.9074 1.5167 2.4166 5.1436 28.0143 1.4597 2.0971 4.2160 25.9822 1.4582 2.3597 4.8364 27.4905 aller EMSE <b>0.85 and <math>p=6</math></b> <b>COMPSE</b> <b>c</b> <sub>3</sub> <b>1.8922</b> 3.0566 7.2244 28.0876 1.5226 2.66216 4.4330	$\begin{array}{c} 2.9743\\ 6.4204\\ 38.3932\\ 1.6707\\ 2.7908\\ 6.1981\\ 36.7776\\ 1.6050\\ 2.3049\\ 5.0250\\ 33.6440\\ 1.5572\\ 2.6470\\ 5.9326\\ 34.2896\\ \hline \\ \hline$	$\begin{array}{c} 1.7514\\ 3.5207\\ 18.2613\\ 1.2051\\ 1.4765\\ 2.7563\\ 10.7996\\ 1.1657\\ 1.4741\\ 2.2270\\ 10.9467\\ 1.2555\\ 1.6952\\ 2.8151\\ 15.5287\\ \hline \\ \hline$	4.3157 22.5578 1.6109 2.2696 3.9640 19.0875 1.5676 1.9301 3.3182 19.6371 1.5249 1.9957 4.0940 18.7061
100 150 200 <u>n</u> 50 100	$\begin{array}{c} 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.95 \\ 0.99 \\ \hline \end{array}$	8.3539 15.0446 82.8496 3.9743 6.6259 13.4735 69.8082 3.7132 5.7822 11.4546 65.2814 3.5341 6.0415 11.8783 61.9594 MLE 5.5244 10.0862 21.7299 97.0780 4.4131 8.0001 13.8590 70.3545	8.0320 14.4979 81.0760 3.9003 6.5054 13.2394 68.7806 3.6685 5.7136 11.3204 64.6202 3.5035 5.9888 11.7739 61.4578 Bol: Table 5: 5.4716 9.9881 21.4923 96.3202 4.3941 7.9648 13.7984 70.0583	1.7971 3.6317 18.7003 1.2142 1.4900 2.7931 10.9614 1.1713 1.4829 2.2450 11.0595 1.2603 1.7040 2.8339 15.6510 d indicated the smather t	2.7803 5.6743 32.9074 1.5167 2.4166 5.1436 28.0143 1.4597 2.0971 4.2160 25.9822 1.4582 2.3597 4.8364 27.4905 aller EMSE <b>COMPSE</b> <b>c</b> <sub>3</sub> <b>1.8922</b> 3.0566 7.2244 28.0876 1.5226 2.66216 4.4330 23.169	$\begin{array}{c} 2.9743\\ 6.4204\\ 38.3932\\ 1.6707\\ 2.7908\\ 6.1981\\ 36.7776\\ 1.6050\\ 2.3049\\ 5.0250\\ 33.6440\\ 1.5572\\ 2.6470\\ 5.9326\\ 34.2896\\ \hline \\ \hline$	1.7514 3.5207 18.2613 1.2051 1.4765 2.7563 10.7996 1.1657 1.4741 2.2270 10.9467 1.2555 1.6952 2.8151 15.5287	4.3157 22.5578 1.6109 2.2696 3.9640 19.0875 1.5676 1.9301 3.3182 19.6371 1.5249 1.9957 4.0940 18.7061
100 150 200 <u>n</u> 50 100	$\begin{array}{c} 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.9 \\ 0.8 \\ 0.8 \\ 0.9 \\ 0.8$	8.3539 15.0446 82.8496 3.9743 6.6259 13.4735 69.8082 3.7132 5.7822 11.4546 65.2814 3.5341 6.0415 11.8783 61.9594 MLE 5.5244 10.0862 21.7299 97.0780 4.4131 8.0001 13.8590 70.3545 4.0898	8.0320 14.4979 81.0760 3.9003 6.5054 13.2394 68.7806 3.6685 5.7136 11.3204 64.6202 3.5035 5.9888 11.7739 61.4578 Bolt <b>Table 5:</b> 7.9648 121.4923 96.3202 4.3941 7.9648 13.7984 70.0583 4.0784	1.7971 3.6317 18.7003 1.2142 1.4900 2.7931 10.9614 1.1713 1.4829 2.2450 11.0595 1.2603 1.7040 2.8339 15.6510 d indicated the smaller EMSEs for $\nu =$ C <sub>2</sub> 1.3559 1.7698 4.0275 12.2767 1.1299 1.5735 2.6634 11.1222 1.1505	2.7803 5.6743 32.9074 1.5167 2.4166 5.1436 28.0143 1.4597 2.0971 4.2160 25.9822 1.4582 2.3597 4.8364 27.4905 aller EMSE <b>COMPSE</b> <b>c</b> <sub>3</sub> <b>1.8922</b> 3.0566 7.2244 28.0876 1.5226 2.66216 4.4330 23.169 1.4857	$\begin{array}{c} 2.9743\\ 6.4204\\ 38.3932\\ 1.6707\\ 2.7908\\ 6.1981\\ 36.7776\\ 1.6050\\ 2.3049\\ 5.0250\\ 33.6440\\ 1.5572\\ 2.6470\\ 5.9326\\ 34.2896\\ \hline \\ \hline$	1.7514 3.5207 18.2613 1.2051 1.4765 2.7563 10.7996 1.1657 1.4741 2.2270 10.9467 1.2555 1.6952 2.8151 15.5287	4.3157 22.5578 1.6109 2.2696 3.9640 19.0875 1.5676 1.9301 3.3182 19.6371 1.5249 1.9957 4.0940 18.7061
100 150 200 n	$\begin{array}{c} 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.95 \\ 0.99 \\ \hline \end{array}$	8.3539 15.0446 82.8496 3.9743 6.6259 13.4735 69.8082 3.7132 5.7822 11.4546 65.2814 3.5341 6.0415 11.8783 61.9594 MLE 5.5244 10.0862 21.7299 97.0780 4.4131 8.0001 13.8590 70.3545	8.0320 14.4979 81.0760 3.9003 6.5054 13.2394 68.7806 3.6685 5.7136 11.3204 64.6202 3.5035 5.9888 11.7739 61.4578 Bol: Table 5: 5.4716 9.9881 21.4923 96.3202 4.3941 7.9648 13.7984 70.0583	1.7971 3.6317 18.7003 1.2142 1.4900 2.7931 10.9614 1.1713 1.4829 2.2450 11.0595 1.2603 1.7040 2.8339 15.6510 d indicated the smather t	2.7803 5.6743 32.9074 1.5167 2.4166 5.1436 28.0143 1.4597 2.0971 4.2160 25.9822 1.4582 2.3597 4.8364 27.4905 aller EMSE <b>COMPSE</b> <b>c</b> <sub>3</sub> <b>1.8922</b> 3.0566 7.2244 28.0876 1.5226 2.66216 4.4330 23.169	$\begin{array}{c} 2.9743\\ 6.4204\\ 38.3932\\ 1.6707\\ 2.7908\\ 6.1981\\ 36.7776\\ 1.6050\\ 2.3049\\ 5.0250\\ 33.6440\\ 1.5572\\ 2.6470\\ 5.9326\\ 34.2896\\ \hline \\ \hline$	1.7514 3.5207 18.2613 1.2051 1.4765 2.7563 10.7996 1.1657 1.4741 2.2270 10.9467 1.2555 1.6952 2.8151 15.5287	4.3157 22.5578 1.6109 2.2696 3.9640 19.0875 1.5676 1.9301 3.3182 19.6371 1.5249 1.9957 4.0940 18.7061
100 150 200 <u>n</u> 50 100	$\begin{array}{c} 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.9 \\ 0.9 \\ 0.9 \\ 0.9 \\ 0.8 \\ 0.9$	8.3539 15.0446 82.8496 3.9743 6.6259 13.4735 69.8082 3.7132 5.7822 11.4546 65.2814 3.5341 6.0415 11.8783 61.9594 MLE 5.5244 10.0862 21.7299 97.0780 4.4131 8.0001 13.8590 70.3545 4.0898 6.7151	8.0320 14.4979 81.0760 3.9003 6.5054 13.2394 68.7806 3.6685 5.7136 11.3204 64.6202 3.5035 5.9888 11.7739 61.4578 Bolt <b>Table 5:</b> 5.4716 9.9881 21.4923 96.3202 4.3941 7.9648 13.7984 13.7984 7.00583 4.0784 6.6967	1.7971 3.6317 18.7003 1.2142 1.4900 2.7931 10.9614 1.1713 1.4829 2.2450 11.0595 1.2603 1.7040 2.8339 15.6510 d indicated the smathering of the state of the smathering of the state of the smathering of the state	2.7803 5.6743 32.9074 1.5167 2.4166 5.1436 28.0143 1.4597 2.0971 4.2160 25.9822 1.4582 2.3597 4.8364 27.4905 2.3597 4.8364 27.4905 2.3597 4.8364 27.4905 2.3597 4.8364 27.4905 2.3597 4.8364 27.4905 2.3597 4.8364 27.4905 2.3597 4.8364 27.4905 2.3597 4.8364 2.3597 4.837 4.837 3.0566 7.2244 2.66216 4.4330 2.3169 1.4857 2.2573	$\begin{array}{c} 2.9743\\ 6.4204\\ 38.3932\\ 1.6707\\ 2.7908\\ 6.1981\\ 36.7776\\ 1.6050\\ 2.3049\\ 5.0250\\ 33.6440\\ 1.5572\\ 2.6470\\ 5.9326\\ 34.2896\\ \hline \end{array}$	1.7514 3.5207 18.2613 1.2051 1.4765 2.7563 10.7996 1.1657 1.4741 2.2270 10.9467 1.2555 1.6952 2.8151 15.5287	4.3157 22.5578 1.6109 2.2696 3.9640 19.0875 1.5676 1.9301 3.3182 19.6371 1.5249 1.9957 4.0940 18.7061
100 150 200 <u>n</u> 50 100	0.9 0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.9 0.95 0.99 0.95 0.99 0.8 0.9 0.95 0.99 0.95 0.99 0.95 0.99 0.95 0.99 0.95 0.99 0.95 0.99 0.95 0.99 0.95 0.99 0.95 0.99 0.95 0.99 0.95 0.99 0.95 0.99 0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.9 0.95 0	8.3539 15.0446 82.8496 3.9743 6.6259 13.4735 69.8082 3.7132 5.7822 11.4546 65.2814 3.5341 6.0415 11.8783 61.9594 MLE 5.5244 10.0862 21.7299 97.0780 4.4131 8.0001 13.8590 70.3545 4.0898 6.7151 11.3812	8.0320 14.4979 81.0760 3.9003 6.5054 13.2394 68.7806 3.6685 5.7136 11.3204 64.6202 3.5035 5.9888 11.7739 61.4578 Bol <b>Table 5:</b> 5.4716 9.9881 21.4923 96.3202 4.3941 7.9648 13.7984 7.00583 4.0784 6.6967 11.3530	1.7971 3.6317 18.7003 1.2142 1.4900 2.7931 10.9614 1.1713 1.4829 2.2450 11.0595 1.2603 1.7040 2.8339 15.6510 d indicated the sma EMSEs for $\nu =$ $\frac{c_2}{1.3559}$ 1.7698 4.0275 12.2767 1.1299 1.5735 2.6634 11.1222 1.1505 1.3993 2.3845	2.7803 5.6743 32.9074 1.5167 2.4166 5.1436 28.0143 1.4597 2.0971 4.2160 25.9822 1.4582 2.3597 4.8364 27.4905 	$\begin{array}{c} 2.9743\\ 6.4204\\ 38.3932\\ 1.6707\\ 2.7908\\ 6.1981\\ 36.7776\\ 1.6050\\ 2.3049\\ 5.0250\\ 33.6440\\ 1.5572\\ 2.6470\\ 5.9326\\ 34.2896\\ \hline \\ \hline \\ \hline \\ \hline \\ 2.0588\\ 3.3763\\ 8.3026\\ 28.1059\\ 1.7268\\ 2.9933\\ 4.4197\\ 26.6673\\ 1.6306\\ 2.5946\\ 4.8588\\ \hline \end{array}$	$1.7514$ 3.5207 18.2613 1.2051 1.4765 2.7563 10.7996 1.1657 1.4741 2.2270 10.9467 1.2555 1.6952 2.8151 15.5287 $c_{5}$ 1.3504 1.7598 3.9910 12.2013 1.1280 1.5696 2.6549 11.0810 1.1492 1.3974 2.3804	$\begin{array}{c} 4.3157\\ 22.5578\\ 1.6109\\ 2.2696\\ 3.9640\\ 19.0875\\ 1.5676\\ 1.9301\\ 3.3182\\ 19.6371\\ 1.5249\\ 1.9957\\ 4.0940\\ 18.7061\\ \hline \end{array}$
100 150 200 <u>n</u> 50 100 150	$\begin{array}{c} 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.95\\ 0.99\\ 0.95\\ 0.99\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.99\\ 0.95\\ 0.99\\ 0.99\\ 0.95\\ 0.99\\ 0.99\\ 0.95\\ 0.99\\ 0.99\\ 0.95\\ 0.99\\ 0.99\\ 0.95\\ 0.99\\ 0.99\\ 0.99\\ 0.95\\ 0.99\\ 0.99\\ 0.99\\ 0.95\\ 0.99\\ 0.99\\ 0.99\\ 0.95\\ 0.99\\ 0.99\\ 0.99\\ 0.95\\ 0.99\\ 0.99\\ 0.95\\ 0.99$	8.3539 15.0446 82.8496 3.9743 6.6259 13.4735 69.8082 3.7132 5.7822 11.4546 65.2814 3.5341 6.0415 11.8783 61.9594 MLE 5.5244 10.0862 21.7299 97.0780 4.4131 8.0001 13.8590 70.3545 4.0898 6.7151 11.3812 64.0067	8.0320 14.4979 81.0760 3.9003 6.5054 13.2394 68.7806 3.6685 5.7136 11.3204 64.6202 3.5035 5.9888 11.7739 61.4578 Bol <b>Table 5:</b> <b>C</b> 1 5.4716 9.9881 21.4923 96.3202 4.3941 7.9648 13.7984 13.7984 13.7984 6.6967 11.3530 63.8508	1.7971 3.6317 18.7003 1.2142 1.4900 2.7931 10.9614 1.1713 1.4829 2.2450 11.0595 1.2603 1.7040 2.8339 15.6510 d indicated the smale <u>C<sub>2</sub></u> 1.3559 1.7698 4.0275 12.2767 1.1299 1.5735 2.6634 11.1222 1.1505 1.3993 2.3845 12.0997	2.7803 5.6743 32.9074 1.5167 2.4166 5.1436 28.0143 1.4597 2.0971 4.2160 25.9822 1.4582 2.3597 4.8364 27.4905 aller EMSE <b>c</b> 0.85 and $p=6$ <b>COMPSE</b> <b>c</b> 3 <b>1.8922</b> 3.0566 7.2244 28.0876 1.5226 2.66216 4.4330 23.169 1.4857 2.2573 4.1255 22.4253	$\begin{array}{c} 2.9743\\ 6.4204\\ 38.3932\\ 1.6707\\ 2.7908\\ 6.1981\\ 36.7776\\ 1.6050\\ 2.3049\\ 5.0250\\ 33.6440\\ 1.5572\\ 2.6470\\ 5.9326\\ 34.2896\\ \hline \\ \hline$	1.7514 3.5207 18.2613 1.2051 1.4765 2.7563 10.7996 1.1657 1.4741 2.2270 10.9467 1.2555 1.6952 2.8151 15.5287	4.3157 22.5578 1.6109 2.2696 3.9640 19.0875 1.5676 1.9301 3.3182 19.6371 1.5249 1.9957 4.0940 18.7061
100 150 200 <u>n</u> 50 100	$\begin{array}{c} 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.95 \\ 0.99 \\ 0.95$	8.3539 15.0446 82.8496 3.9743 6.6259 13.4735 69.8082 3.7132 5.7822 11.4546 65.2814 3.5341 6.0415 11.8783 61.9594 MLE 5.5244 10.0862 21.7299 97.0780 4.4131 8.0001 13.8590 70.3545 4.0898 6.7151 11.3812	8.0320 14.4979 81.0760 3.9003 6.5054 13.2394 68.7806 3.6685 5.7136 11.3204 64.6202 3.5035 5.9888 11.7739 61.4578 Bol <b>Table 5:</b> <b>C</b> 1 5.4716 9.9881 21.4923 96.3202 4.3941 7.9648 13.7984 7.9648 13.7984 7.9648 13.7984 7.90583 4.0784 6.6967 11.3530 63.8508 3.5991	1.7971 3.6317 18.7003 1.2142 1.4900 2.7931 10.9614 1.1713 1.4829 2.2450 11.0595 1.2603 1.7040 2.8339 15.6510 d indicated the sma EMSEs for $\nu =$ $\frac{c_2}{1.3559}$ 1.7698 4.0275 12.2767 1.1299 1.5735 2.6634 11.1222 1.1505 1.3993 2.3845	2.7803 5.6743 32.9074 1.5167 2.4166 5.1436 28.0143 1.4597 2.0971 4.2160 25.9822 1.4582 2.3597 4.8364 27.4905 aller EMSE <b>0.85 and <math>p=6</math></b> <b>COMPSE</b> <b>c</b> <sub>3</sub> <b>1.8922</b> 3.0566 7.2244 28.0876 1.5226 2.66216 4.4330 23.169 1.4857 2.2573 4.1255 22.4253 1.3149	$\begin{array}{c} 2.9743\\ 6.4204\\ 38.3932\\ 1.6707\\ 2.7908\\ 6.1981\\ 36.7776\\ 1.6050\\ 2.3049\\ 5.0250\\ 33.6440\\ 1.5572\\ 2.6470\\ 5.9326\\ 34.2896\\ \hline \\ \hline$	$1.7514$ 3.5207 18.2613 1.2051 1.4765 2.7563 10.7996 1.1657 1.4741 2.2270 10.9467 1.2555 1.6952 2.8151 15.5287 $c_{5}$ 1.3504 1.7598 3.9910 12.2013 1.1280 1.5696 2.6549 11.0810 1.1492 1.3974 2.3804	4.3157 22.5578 1.6109 2.2696 3.9640 19.0875 1.5676 1.9301 3.3182 19.6371 1.5249 1.9957 4.0940 18.7061
100 150 200 <u>n</u> 50 100 150	$\begin{array}{c} 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.95\\ 0.99\\ 0.95\\ 0.99\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.99\\ 0.95\\ 0.99\\ 0.99\\ 0.95\\ 0.99\\ 0.99\\ 0.95\\ 0.99\\ 0.99\\ 0.95\\ 0.99\\ 0.99\\ 0.95\\ 0.99\\ 0.99\\ 0.99\\ 0.95\\ 0.99\\ 0.99\\ 0.99\\ 0.95\\ 0.99\\ 0.99\\ 0.99\\ 0.95\\ 0.99\\ 0.99\\ 0.99\\ 0.95\\ 0.99\\ 0.99\\ 0.95\\ 0.99$	8.3539 15.0446 82.8496 3.9743 6.6259 13.4735 69.8082 3.7132 5.7822 11.4546 65.2814 3.5341 6.0415 11.8783 61.9594 MLE 5.5244 10.0862 21.7299 97.0780 4.4131 8.0001 13.8590 70.3545 4.0898 6.7151 11.3812 64.0067	8.0320 14.4979 81.0760 3.9003 6.5054 13.2394 68.7806 3.6685 5.7136 11.3204 64.6202 3.5035 5.9888 11.7739 61.4578 Bol <b>Table 5:</b> <b>C</b> 1 5.4716 9.9881 21.4923 96.3202 4.3941 7.9648 13.7984 13.7984 13.7984 6.6967 11.3530 63.8508	1.7971 3.6317 18.7003 1.2142 1.4900 2.7931 10.9614 1.1713 1.4829 2.2450 11.0595 1.2603 1.7040 2.8339 15.6510 d indicated the smale <u>C<sub>2</sub></u> 1.3559 1.7698 4.0275 12.2767 1.1299 1.5735 2.6634 11.1222 1.1505 1.3993 2.3845 12.0997	2.7803 5.6743 32.9074 1.5167 2.4166 5.1436 28.0143 1.4597 2.0971 4.2160 25.9822 1.4582 2.3597 4.8364 27.4905 aller EMSE <b>c</b> 0.85 and $p=6$ <b>COMPSE</b> <b>c</b> 3 <b>1.8922</b> 3.0566 7.2244 28.0876 1.5226 2.66216 4.4330 23.169 1.4857 2.2573 4.1255 22.4253	$\begin{array}{c} 2.9743\\ 6.4204\\ 38.3932\\ 1.6707\\ 2.7908\\ 6.1981\\ 36.7776\\ 1.6050\\ 2.3049\\ 5.0250\\ 33.6440\\ 1.5572\\ 2.6470\\ 5.9326\\ 34.2896\\ \hline \\ \hline$	1.7514 3.5207 18.2613 1.2051 1.4765 2.7563 10.7996 1.1657 1.4741 2.2270 10.9467 1.2555 1.6952 2.8151 15.5287	4.3157 22.5578 1.6109 2.2696 3.9640 19.0875 1.5676 1.9301 3.3182 19.6371 1.5249 1.9957 4.0940 18.7061
100 150 200 <u>n</u> 50 100 150	$\begin{array}{c} 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.95 \\ 0.99 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.9 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.9 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.9 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.9 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.9 \\ 0.9 \\ 0.9 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0$	8.3539 15.0446 82.8496 3.9743 6.6259 13.4735 69.8082 3.7132 5.7822 11.4546 65.2814 3.5341 6.0415 11.8783 61.9594	8.0320 14.4979 81.0760 3.9003 6.5054 13.2394 68.7806 3.6685 5.7136 11.3204 64.6202 3.5035 5.9888 11.7739 61.4578 Bol: Table 5: C1 5.4716 9.9881 21.4923 96.3202 4.3941 7.9648 13.7984 7.9648 13.7984 7.0583 4.0784 6.6967 11.3530 63.8508 3.5991 6.8991	1.7971 3.6317 18.7003 1.2142 1.4900 2.7931 10.9614 1.1713 1.4829 2.2450 11.0595 1.2603 1.7040 2.8339 15.6510 d indicated the smather t	2.7803 5.6743 32.9074 1.5167 2.4166 5.1436 28.0143 1.4597 2.0971 4.2160 25.9822 1.4582 2.3597 4.8364 27.4905 aller EMSE <b>COMPSE</b> <b>c</b> <sub>3</sub> <b>1.8922</b> 3.0566 7.2244 28.0876 1.5226 2.66216 4.4330 23.169 1.4857 2.2573 4.1255 22.4253 1.3149 2.5376	$\begin{array}{c} 2.9743\\ 6.4204\\ 38.3932\\ 1.6707\\ 2.7908\\ 6.1981\\ 36.7776\\ 1.6050\\ 2.3049\\ 5.0250\\ 33.6440\\ 1.5572\\ 2.6470\\ 5.9326\\ 34.2896\\ \hline \end{array}$	1.7514 3.5207 18.2613 1.2051 1.4765 2.7563 10.7996 1.1657 1.4741 2.2270 10.9467 1.2555 1.6952 2.8151 15.5287	4.3157 22.5578 1.6109 2.2696 3.9640 19.0875 1.5676 1.9301 3.3182 19.6371 1.5249 1.9957 4.0940 18.7061
100 150 200 <u>n</u> 50 100 150	$\begin{array}{c} 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.95 \\ 0.99 \\ 0.95$	8.3539 15.0446 82.8496 3.9743 6.6259 13.4735 69.8082 3.7132 5.7822 11.4546 65.2814 3.5341 6.0415 11.8783 61.9594	8.0320 14.4979 81.0760 3.9003 6.5054 13.2394 68.7806 3.6685 5.7136 11.3204 64.6202 3.5035 5.9888 11.7739 61.4578 Bol <b>Table 5:</b> <b>C</b> 1 5.4716 9.9881 21.4923 96.3202 4.3941 7.9648 13.7984 7.9648 13.7984 7.9648 13.7984 7.90583 4.0784 6.6967 11.3530 63.8508 3.5991	1.7971 3.6317 18.7003 1.2142 1.4900 2.7931 10.9614 1.1713 1.4829 2.2450 11.0595 1.2603 1.7040 2.8339 15.6510 d indicated the smather t	2.7803 5.6743 32.9074 1.5167 2.4166 5.1436 28.0143 1.4597 2.0971 4.2160 25.9822 1.4582 2.3597 4.8364 27.4905 aller EMSE <b>0.85 and <math>p=6</math></b> <b>COMPSE</b> <b>c</b> <sub>3</sub> <b>1.8922</b> 3.0566 7.2244 28.0876 1.5226 2.66216 4.4330 23.169 1.4857 2.2573 4.1255 22.4253 1.3149	$\begin{array}{c} 2.9743\\ 6.4204\\ 38.3932\\ 1.6707\\ 2.7908\\ 6.1981\\ 36.7776\\ 1.6050\\ 2.3049\\ 5.0250\\ 33.6440\\ 1.5572\\ 2.6470\\ 5.9326\\ 34.2896\\ \hline \\ \hline$	1.7514 3.5207 18.2613 1.2051 1.4765 2.7563 10.7996 1.1657 1.4741 2.2270 10.9467 1.2555 1.6952 2.8151 15.5287	4.3157 22.5578 1.6109 2.2696 3.9640 19.0875 1.5676 1.9301 3.3182 19.6371 1.5249 1.9957 4.0940 18.7061

**Table 6:** EMSEs for v = 1 and p=6

n					COMPCE			
	$\rho^2$ -				COMPSE			
	-	MLE	<i>C</i> <sub>1</sub>	<i>c</i> <sub>2</sub> 1.2930	<i>c</i> <sub>3</sub> 2.2997	C <sub>4</sub>	<i>C</i> <sub>5</sub>	<i>C</i> <sub>6</sub>
50	0.8	9.7380	9.5465	1.2930	2.2997	2.2568	1.2812	2.6322
	0.9	16.7992	16.4948	2.4856	4.6955	4.7940	2.4543	4.9610
	0.95	29.3329	28.7969	3.3275	7.3523	7.0641	3.2781	7.0416
	0.99	158.2569	156.1642	16.2835	40.8691	34.8033	16.0679	36.7931
100	0.8	5.4680	5.4195	1.0782	1.5418	1.5392	1.0753	1.8331
100	0.0							1.0551
	0.9	10.8507	10.7598	1.8176	3.1737	3.4687	1.8089	3.5306
	0.95	19.6763	19.5097	3.1715	5.6516	5.3441	3.1510	5.9439
	0.99	102.6834	101.993	14.5491	31.1315	29.3552	14.4592	30.7586
150	0.8	4.8208	4.7946	1.1193	1.5207	1.6000	1.1171	1.8253
	0.9	8.2393	8.1952	1.3440	2.2222	2.1182	1.3409	2.5607
	0.95	18.2975	18.1992	2.7970	5.4004	5.3754	2.7861	5.9125
	0.95				3.4004			
	0.99	88.0189	87.5731	12.8577	25.7513	24.5624	12.7971	26.6877
200	0.8	4.5940	4.5759	1.0258	1.3803	1.3820	1.0247	1.6945
	0.9	10.0725	10.0327	1.8709	3.0711	3.2428	1.8663	3.6242
	0.95	16.2784	16.2148	2.3754	4.8462	4.9285	2.3688	5.7353
	0.99	73.5241	73.2503	9.5098	21.1291	21.1951	9.4776	21.0472
	0.77	70.0211		old indicated the sm		21.1701	,,,,,,	21.01/2
			ים	olu mulcateu tile sii				
			Table 7	<b>7:</b> EMSEs for $\nu$ =				
n	$\rho^2$				COMPSE			
		MLE	<i>c</i> <sub>1</sub>	<i>C</i> <sub>2</sub>	<i>C</i> <sub>3</sub>	<i>C</i> <sub>4</sub>	C <sub>5</sub>	C <sub>6</sub>
50	0.8	12.4644	11.9755	1.6703	2.8483	2.7768	1.6299	3.0068
	0.9	24.1352	23.2601	2.6034	5.5108	4.7107	2.5360	5.0147
	0.95	43.8464	42.3519	4.0853	9.6509	7.2007	3.9730	8.0726
	0.99	242.5266	237.045	23.7372	57.3941	50.6290	23.1779	45.0071
100	0.8	8.5819	8.4198	1.2109	2.0600	1.9042	1.2029	2.1939
100	0.0							
	0.9	16.8357	16.5257	2.1273	4.1330	3.8733	2.1009	4.0861
	0.95	29.1483	28.6094	3.0947	6.6175	5.5064	3.0514	5.7289
	0.99	143.819	141.6595	13.1633	34.3678	27.7705	12.9960	28.6092
150	0.8	7.9381	7.8411	1.2152	1.9477	1.8511	1.2099	2.1776
	0.9	14.2010	14.0362	1.7782	3.5553	3.5147	1.7672	3.7716
	0.95	27.8953	27.5761	3.3276	6.8072	5.5076	3.2995	6.6319
	0.95	125.6663	124.3192			21.8648		
200				10.7117	29.5072		10.6022	23.5085
200	0.8	8.1053	8.0344	1.4329	2.1181	2.0163	1.4272	2.3321
	0.9	14.8690	14.7396	2.1142	3.8277	3.5558	2.1021	3.9285
	0.95	21.4289	21.2401	2.0310	4.7601	4.3053	2.0201	4.3892
	0.99	129.477	128.5728	10.4659	29.9874	23.5663	10.3983	30.4567
			B	old indicated the sm	aller EMSE			
			Table 8	<b>B:</b> EMSEs for $\nu$ =	- 0.85 and <i>n</i> =9			
	2			<b>.</b> LINSES IOT / -	COMPSE			
п	$ ho^2$	MLE	<i>c</i> <sub>1</sub>	<i>C</i> <sub>2</sub>	C <sub>3</sub>	C <sub>4</sub>	<i>C</i> <sub>5</sub>	<i>C</i> <sub>6</sub>
50	0.8	12.1742	12.0412	1.6200	3.0387	3.1966	1.6104	4.0494
	0.9	20.1100	19.8980	2.4295	4.8852	5.0000	2.4120	6.1762
	0.95			4.7000				
		44.9510	44.4881	4.7080	11.5664	11.5920	4.6714	13.3608
	0.99	189.7279	188.2678	15.8642	45.5422	43.5135	15.7598	46.8489
100	0.8		7.9266	1.3268	2.1726	2.1689	1.3240	2.9569
		7.9619	7.9200			4 00 4 0		
	0.9	7.9619 15.27	15.1989	1.9019	3.9662	4.0940	1.8964	5.3999
		15.27	15.1989	1.9019				5.3999
	0.95	15.27 27.2705	15.1989 27.1466	1.9019 3.1270	6.6739	6.1911	3.1166	5.3999 8.7935
150	0.95 0.99	15.27 27.2705 131.5003	15.1989 27.1466 131.0075	1.9019 3.1270 15.3322	6.6739 35.2562	6.1911 36.1952	3.1166 15.2779	5.3999 8.7935 42.0009
150	0.95 0.99 0.8	15.27 27.2705 131.5003 8.9205	15.1989 27.1466 131.0075 8.8954	1.9019 3.1270 15.3322 1.4012	6.6739 35.2562 2.4713	6.1911 36.1952 2.4747	3.1166 15.2779 1.3993	5.3999 8.7935 42.0009 3.3992
150	0.95 0.99 0.8 0.9	15.27 27.2705 131.5003 8.9205 14.1834	15.1989 27.1466 131.0075 8.8954 14.1451	1.9019 3.1270 15.3322 1.4012 2.1094	6.6739 35.2562 2.4713 3.8912	6.1911 36.1952 2.4747 3.9483	3.1166 15.2779 1.3993 2.1058	5.3999 8.7935 42.0009 3.3992 5.2536
150	0.95 0.99 0.8 0.9 0.95	15.27 27.2705 131.5003 8.9205 14.1834 30.6178	15.1989 27.1466 131.0075 8.8954	1.9019 3.1270 15.3322 1.4012	6.6739 35.2562 2.4713 3.8912 8.6451	6.1911 36.1952 2.4747	3.1166 15.2779 1.3993	5.3999 8.7935 42.0009 3.3992 5.2536 11.1534
150	0.95 0.99 0.8 0.9	15.27 27.2705 131.5003 8.9205 14.1834	15.1989 27.1466 131.0075 8.8954 14.1451	1.9019 3.1270 15.3322 1.4012 2.1094	6.6739 35.2562 2.4713 3.8912	6.1911 36.1952 2.4747 3.9483	3.1166 15.2779 1.3993 2.1058	5.3999 8.7935 42.0009 3.3992 5.2536
	0.95 0.99 0.8 0.9 0.95 0.99	$\begin{array}{c} 15.27\\ 27.2705\\ 131.5003\\ 8.9205\\ 14.1834\\ 30.6178\\ 157.0304\end{array}$	15.1989 27.1466 131.0075 8.8954 14.1451 30.5325 156.641	1.9019 3.1270 15.3322 1.4012 2.1094 4.4406 19.0963	6.6739 35.2562 2.4713 3.8912 8.6451 42.8419	6.1911 36.1952 2.4747 3.9483 8.6224 43.4421	3.1166 15.2779 1.3993 2.1058 4.4303 19.0511	5.3999 8.7935 42.0009 3.3992 5.2536 11.1534 56.3899
150 200	0.95 0.99 0.8 0.9 0.95 0.99 0.8	$\begin{array}{c} 15.27\\ 27.2705\\ 131.5003\\ 8.9205\\ 14.1834\\ 30.6178\\ 157.0304\\ 7.6837\end{array}$	$\begin{array}{c} 15.1989\\ 27.1466\\ 131.0075\\ 8.8954\\ 14.1451\\ 30.5325\\ 156.641\\ 7.6684\end{array}$	$\begin{array}{c} 1.9019\\ 3.1270\\ 15.3322\\ 1.4012\\ 2.1094\\ 4.4406\\ 19.0963\\ 1.3629\end{array}$	6.6739 35.2562 2.4713 3.8912 8.6451 42.8419 2.2028	6.1911 36.1952 2.4747 3.9483 8.6224 43.4421 2.3043	3.1166 15.2779 1.3993 2.1058 4.4303 19.0511 1.3616	5.3999 8.7935 42.0009 3.3992 5.2536 11.1534 56.3899 3.1764
	0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.9	$\begin{array}{c} 15.27\\ 27.2705\\ 131.5003\\ 8.9205\\ 14.1834\\ 30.6178\\ 157.0304\\ 7.6837\\ 15.4263\end{array}$	$\begin{array}{c} 15.1989\\ 27.1466\\ 131.0075\\ 8.8954\\ 14.1451\\ 30.5325\\ 156.641\\ 7.6684\\ 15.3952\end{array}$	$\begin{array}{c} 1.9019\\ 3.1270\\ 15.3322\\ 1.4012\\ 2.1094\\ 4.4406\\ 19.0963\\ 1.3629\\ 2.1455\end{array}$	6.6739 35.2562 2.4713 3.8912 8.6451 42.8419 2.2028 4.5035	$\begin{array}{c} 6.1911\\ 36.1952\\ 2.4747\\ 3.9483\\ 8.6224\\ 43.4421\\ 2.3043\\ 5.0588\end{array}$	3.1166 15.2779 1.3993 2.1058 4.4303 19.0511 1.3616 2.1426	5.3999 8.7935 42.0009 3.3992 5.2536 11.1534 56.3899 3.1764 6.1252
	0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.9 0.9	$\begin{array}{c} 15.27\\ 27.2705\\ 131.5003\\ 8.9205\\ 14.1834\\ 30.6178\\ 157.0304\\ 7.6837\\ 15.4263\\ 28.4487\end{array}$	$\begin{array}{c} 15.1989\\ 27.1466\\ 131.0075\\ 8.8954\\ 14.1451\\ 30.5325\\ 156.641\\ 7.6684\\ 15.3952\\ 28.3901 \end{array}$	$\begin{array}{c} 1.9019\\ 3.1270\\ 15.3322\\ 1.4012\\ 2.1094\\ 4.4406\\ 19.0963\\ 1.3629\\ 2.1455\\ 3.8966\end{array}$	6.6739 35.2562 2.4713 3.8912 8.6451 42.8419 2.2028 4.5035 7.9984	$\begin{array}{c} 6.1911\\ 36.1952\\ 2.4747\\ 3.9483\\ 8.6224\\ 43.4421\\ 2.3043\\ 5.0588\\ 8.1217\end{array}$	3.1166 15.2779 1.3993 2.1058 4.4303 19.0511 1.3616 2.1426 3.8902	5.3999 8.7935 42.0009 3.3992 5.2536 11.1534 56.3899 3.1764 6.1252 10.5169
	0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.9	$\begin{array}{c} 15.27\\ 27.2705\\ 131.5003\\ 8.9205\\ 14.1834\\ 30.6178\\ 157.0304\\ 7.6837\\ 15.4263\end{array}$	$\begin{array}{c} 15.1989\\ 27.1466\\ 131.0075\\ 8.8954\\ 14.1451\\ 30.5325\\ 156.641\\ 7.6684\\ 15.3952\\ 28.3901\\ 142.7522\end{array}$	$\begin{array}{c} 1.9019\\ 3.1270\\ 15.3322\\ 1.4012\\ 2.1094\\ 4.4406\\ 19.0963\\ 1.3629\\ 2.1455\\ 3.8966\\ 16.3336\end{array}$	6.6739 35.2562 2.4713 3.8912 8.6451 42.8419 2.2028 4.5035 7.9984 39.3749	$\begin{array}{c} 6.1911\\ 36.1952\\ 2.4747\\ 3.9483\\ 8.6224\\ 43.4421\\ 2.3043\\ 5.0588\end{array}$	3.1166 15.2779 1.3993 2.1058 4.4303 19.0511 1.3616 2.1426	5.3999 8.7935 42.0009 3.3992 5.2536 11.1534 56.3899 3.1764 6.1252
	0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.9 0.9	$\begin{array}{c} 15.27\\ 27.2705\\ 131.5003\\ 8.9205\\ 14.1834\\ 30.6178\\ 157.0304\\ 7.6837\\ 15.4263\\ 28.4487\end{array}$	15.1989 27.1466 131.0075 8.8954 14.1451 30.5325 156.641 7.6684 15.3952 28.3901 142.7522 B	1.9019 3.1270 15.3322 1.4012 2.1094 4.4406 19.0963 1.3629 2.1455 3.8966 16.3336 old indicated the sn	6.6739 35.2562 2.4713 3.8912 8.6451 42.8419 2.2028 4.5035 7.9984 39.3749 maller EMSE	$\begin{array}{c} 6.1911\\ 36.1952\\ 2.4747\\ 3.9483\\ 8.6224\\ 43.4421\\ 2.3043\\ 5.0588\\ 8.1217\end{array}$	3.1166 15.2779 1.3993 2.1058 4.4303 19.0511 1.3616 2.1426 3.8902	5.3999 8.7935 42.0009 3.3992 5.2536 11.1534 56.3899 3.1764 6.1252 10.5169
	0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.9 0.9	$\begin{array}{c} 15.27\\ 27.2705\\ 131.5003\\ 8.9205\\ 14.1834\\ 30.6178\\ 157.0304\\ 7.6837\\ 15.4263\\ 28.4487\end{array}$	15.1989 27.1466 131.0075 8.8954 14.1451 30.5325 156.641 7.6684 15.3952 28.3901 142.7522 B	$\begin{array}{c} 1.9019\\ 3.1270\\ 15.3322\\ 1.4012\\ 2.1094\\ 4.4406\\ 19.0963\\ 1.3629\\ 2.1455\\ 3.8966\\ 16.3336\end{array}$	6.6739 35.2562 2.4713 3.8912 8.6451 42.8419 2.2028 4.5035 7.9984 39.3749 maller EMSE v = 1 and $p=9$	$\begin{array}{c} 6.1911\\ 36.1952\\ 2.4747\\ 3.9483\\ 8.6224\\ 43.4421\\ 2.3043\\ 5.0588\\ 8.1217\end{array}$	3.1166 15.2779 1.3993 2.1058 4.4303 19.0511 1.3616 2.1426 3.8902	5.3999 8.7935 42.0009 3.3992 5.2536 11.1534 56.3899 3.1764 6.1252 10.5169
	$\begin{array}{c} 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.95 \\ 0.99 \\ 0.95 \\ 0.99 \end{array}$	$\begin{array}{c} 15.27\\ 27.2705\\ 131.5003\\ 8.9205\\ 14.1834\\ 30.6178\\ 157.0304\\ 7.6837\\ 15.4263\\ 28.4487\\ 143.018\end{array}$	15.1989 27.1466 131.0075 8.8954 14.1451 30.5325 156.641 7.6684 15.3952 28.3901 142.7522 B <b>Table</b>	1.9019 3.1270 15.3322 1.4012 2.1094 4.4406 19.0963 1.3629 2.1455 3.8966 16.3336 old indicated the sn	6.6739 35.2562 2.4713 3.8912 8.6451 42.8419 2.2028 4.5035 7.9984 39.3749 maller EMSE p = 1 and $p=9COMPSE$	6.1911 36.1952 2.4747 3.9483 8.6224 43.4421 2.3043 5.0588 8.1217 41.3574	3.1166 15.2779 1.3993 2.1058 4.4303 19.0511 1.3616 2.1426 3.8902 16.3061	5.3999 8.7935 42.0009 3.3992 5.2536 11.1534 56.3899 3.1764 6.1252 10.5169 51.0804
200 n	$\begin{array}{c} 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.95\\ 0.99\\ \end{array}$	15.27 27.2705 131.5003 8.9205 14.1834 30.6178 157.0304 7.6837 15.4263 28.4487 143.018 MLE	15.1989 27.1466 131.0075 8.8954 14.1451 30.5325 156.641 7.6684 15.3952 28.3901 142.7522 B <b>Table</b>	1.9019 3.1270 15.3322 1.4012 2.1094 4.4406 19.0963 1.3629 2.1455 3.8966 16.3336 old indicated the sn <b>e 9: EMSEs for 1</b> <i>C</i> <sub>2</sub>	$\begin{array}{c} 6.6739\\ 35.2562\\ 2.4713\\ 3.8912\\ 8.6451\\ 42.8419\\ 2.2028\\ 4.5035\\ 7.9984\\ 39.3749\\ \hline \\ 39.3749\\ \hline \\ \text{taller EMSE}\\ \hline r=1 \text{ and }p=9\\ \hline \\ \hline \\ \hline \\ COMPSE\\ \hline \\ \hline \\ c_3\\ \end{array}$	6.1911 36.1952 2.4747 3.9483 8.6224 43.4421 2.3043 5.0588 8.1217 41.3574	3.1166 15.2779 1.3993 2.1058 4.4303 19.0511 1.3616 2.1426 3.8902 16.3061	$5.3999 \\ 8.7935 \\ 42.0009 \\ 3.3992 \\ 5.2536 \\ 11.1534 \\ 56.3899 \\ 3.1764 \\ 6.1252 \\ 10.5169 \\ 51.0804 \\ \hline \\ c_6$
200	$\begin{array}{c} 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ \hline \end{array}$	15.27 27.2705 131.5003 8.9205 14.1834 30.6178 157.0304 7.6837 15.4263 28.4487 143.018 MLE 18.2156	15.1989 27.1466 131.0075 8.8954 14.1451 30.5325 156.641 7.6684 15.3952 28.3901 142.7522 B <b>Table</b> <u>c<sub>1</sub></u> 17.8366	$\begin{array}{c} 1.9019\\ 3.1270\\ 15.3322\\ 1.4012\\ 2.1094\\ 4.4406\\ 19.0963\\ 1.3629\\ 2.1455\\ 3.8966\\ 16.3336\\ 0 d indicated the sn\\ e 9: EMSEs for 12\\ \hline c_2\\ 1.6494 \end{array}$	$\begin{array}{c} 6.6739\\ 35.2562\\ 2.4713\\ 3.8912\\ 8.6451\\ 42.8419\\ 2.2028\\ 4.5035\\ 7.9984\\ 39.3749\\ \text{maller EMSE}\\ r=1 \text{ and } p=9\\ \hline \text{COMPSE}\\ \hline c_3\\ \hline 3.5982 \end{array}$	$\begin{array}{c} 6.1911\\ 36.1952\\ 2.4747\\ 3.9483\\ 8.6224\\ 43.4421\\ 2.3043\\ 5.0588\\ 8.1217\\ 41.3574\\ \hline \\ \hline$	3.1166 15.2779 1.3993 2.1058 4.4303 19.0511 1.3616 2.1426 3.8902 16.3061	$5.3999 \\ 8.7935 \\ 42.0009 \\ 3.3992 \\ 5.2536 \\ 11.1534 \\ 56.3899 \\ 3.1764 \\ 6.1252 \\ 10.5169 \\ 51.0804 \\ \hline \\ $
200 n	$\begin{array}{c} 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ \end{array}$	15.27 27.2705 131.5003 8.9205 14.1834 30.6178 157.0304 7.6837 15.4263 28.4487 143.018 MLE 18.2156 30.5285	15.1989 27.1466 131.0075 8.8954 14.1451 30.5325 156.641 7.6684 15.3952 28.3901 142.7522 B <b>Table</b> <u>c<sub>1</sub></u> 17.8366 29.9479	$\begin{array}{c} 1.9019\\ 3.1270\\ 15.3322\\ 1.4012\\ 2.1094\\ 4.4406\\ 19.0963\\ 1.3629\\ 2.1455\\ 3.8966\\ 16.3336\\ 0 d indicated the sn\\ e 9: EMSEs for u\\ \hline \hline c_2\\ 1.6494\\ 2.8947\\ \end{array}$	$\begin{array}{r} 6.6739\\ 35.2562\\ 2.4713\\ 3.8912\\ 8.6451\\ 42.8419\\ 2.2028\\ 4.5035\\ 7.9984\\ 39.3749\\ \text{maller EMSE}\\ p=1 \text{ and } p=9\\ \hline comPSE\\ \hline c_3\\ 3.5982\\ 6.4574\\ \end{array}$	$\begin{array}{c} 6.1911\\ 36.1952\\ 2.4747\\ 3.9483\\ 8.6224\\ 43.4421\\ 2.3043\\ 5.0588\\ 8.1217\\ 41.3574\\ \hline \\ \hline$	$3.116615.27791.39932.10584.430319.05111.36162.14263.890216.3061\hline c_5 \\ 1.6304 \\ 2.8567$	5.3999 8.7935 42.0009 3.3992 5.2536 11.1534 56.3899 3.1764 6.1252 10.5169 51.0804
200 n	$\begin{array}{c} 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ \hline\\ \rho^2 \\ \hline\\ 0.8\\ 0.9\\ 0.95\\ \hline\end{array}$	15.27 27.2705 131.5003 8.9205 14.1834 30.6178 157.0304 7.6837 15.4263 28.4487 143.018 MLE 18.2156	15.1989 27.1466 131.0075 8.8954 14.1451 30.5325 156.641 7.6684 15.3952 28.3901 142.7522 B <b>Table</b> 217.8366 29.9479 56.0273	1.9019 3.1270 15.3322 1.4012 2.1094 4.4406 19.0963 1.3629 2.1455 3.8966 16.3336 old indicated the sn <b>2.9: EMSEs for v</b> <b>c</b> <sub>2</sub> 1.6494 2.8947 3.8033	$\begin{array}{r} 6.6739\\ 35.2562\\ 2.4713\\ 3.8912\\ 8.6451\\ 42.8419\\ 2.2028\\ 4.5035\\ 7.9984\\ 39.3749\\ \text{maller EMSE}\\ \hline p = 1 \text{ and } p=9\\ \hline comPSE\\ \hline c_3\\ 3.5982\\ 6.4574\\ 11.2609\\ \end{array}$	$\begin{array}{c} 6.1911\\ 36.1952\\ 2.4747\\ 3.9483\\ 8.6224\\ 43.4421\\ 2.3043\\ 5.0588\\ 8.1217\\ 41.3574\\ \hline \\ \hline$	3.1166 15.2779 1.3993 2.1058 4.4303 19.0511 1.3616 2.1426 3.8902 16.3061	$5.3999 \\ 8.7935 \\ 42.0009 \\ 3.3992 \\ 5.2536 \\ 11.1534 \\ 56.3899 \\ 3.1764 \\ 6.1252 \\ 10.5169 \\ 51.0804 \\ \hline \\ \hline \\ \hline \\ \hline \\ \hline \\ \\ \\ \hline \\$
200 n	$\begin{array}{c} 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ \end{array}$	15.27 27.2705 131.5003 8.9205 14.1834 30.6178 157.0304 7.6837 15.4263 28.4487 143.018 MLE 18.2156 30.5285	15.1989 27.1466 131.0075 8.8954 14.1451 30.5325 156.641 7.6684 15.3952 28.3901 142.7522 B <b>Table</b> <u>c<sub>1</sub></u> 17.8366 29.9479	$\begin{array}{c} 1.9019\\ 3.1270\\ 15.3322\\ 1.4012\\ 2.1094\\ 4.4406\\ 19.0963\\ 1.3629\\ 2.1455\\ 3.8966\\ 16.3336\\ 0 d indicated the sn\\ e 9: EMSEs for u\\ \hline \hline c_2\\ 1.6494\\ 2.8947\\ \end{array}$	$\begin{array}{r} 6.6739\\ 35.2562\\ 2.4713\\ 3.8912\\ 8.6451\\ 42.8419\\ 2.2028\\ 4.5035\\ 7.9984\\ 39.3749\\ \text{maller EMSE}\\ \textbf{v} = 1 \text{ and } p=9\\ \hline comPSE\\ \hline c_3\\ 3.5982\\ 6.4574 \end{array}$	$\begin{array}{c} 6.1911\\ 36.1952\\ 2.4747\\ 3.9483\\ 8.6224\\ 43.4421\\ 2.3043\\ 5.0588\\ 8.1217\\ 41.3574\\ \hline \\ \hline$	$3.116615.27791.39932.10584.430319.05111.36162.14263.890216.3061\hline c_5 \\ 1.6304 \\ 2.8567$	5.3999 8.7935 42.0009 3.3992 5.2536 11.1534 56.3899 3.1764 6.1252 10.5169 51.0804
200 n 50	$\begin{array}{c} 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ \hline\\ \end{array}$	15.27 27.2705 131.5003 8.9205 14.1834 30.6178 157.0304 7.6837 15.4263 28.4487 143.018 MLE 18.2156 30.5285 57.0240 315.518	15.1989 27.1466 131.0075 8.8954 14.1451 30.5325 156.641 7.6684 15.3952 28.3901 142.7522 B <b>Table</b> <u>C<sub>1</sub></u> 17.8366 29.9479 56.0273 312.7813	$\begin{array}{c} 1.9019\\ 3.1270\\ 15.3322\\ 1.4012\\ 2.1094\\ 4.4406\\ 19.0963\\ 1.3629\\ 2.1455\\ 3.8966\\ 16.3336\\ 0ld indicated the sn\\ e 9: EMSEs for v\\ \hline \hline c_2\\ 1.6494\\ 2.8947\\ 3.8033\\ 26.6251\\ \end{array}$	$\begin{array}{c} 6.6739\\ 35.2562\\ 2.4713\\ 3.8912\\ 8.6451\\ 42.8419\\ 2.2028\\ 4.5035\\ 7.9984\\ 39.3749\\ \hline \\ abler EMSE\\ \hline \\ r = 1 \ and \ p=9\\ \hline \\ \hline \\ \hline \\ compse\\ \hline \\ c_3\\ \hline \\ 3.5982\\ 6.4574\\ 11.2609\\ 69.7525\\ \hline \end{array}$	$\begin{array}{c} 6.1911\\ 36.1952\\ 2.4747\\ 3.9483\\ 8.6224\\ 43.4421\\ 2.3043\\ 5.0588\\ 8.1217\\ 41.3574\\ \hline \\ \hline$	$\begin{array}{c} 3.1166\\ 15.2779\\ 1.3993\\ 2.1058\\ 4.4303\\ 19.0511\\ 1.3616\\ 2.1426\\ 3.8902\\ 16.3061\\ \hline \\ \hline$	5.3999 8.7935 42.0009 3.3992 5.2536 11.1534 56.3899 3.1764 6.1252 10.5169 51.0804 <u>c_6</u> 4.1569 7.1828 12.9065 72.2782
200 n 50	$\begin{array}{c} 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ \hline\\ \rho^2 \\ \hline\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ \hline\end{array}$	15.27 27.2705 131.5003 8.9205 14.1834 30.6178 157.0304 7.6837 15.4263 28.4487 143.018 <u>MLE</u> 18.2156 30.5285 57.0240 315.518 11.8646	$\begin{array}{c} 15.1989\\ 27.1466\\ 131.0075\\ 8.8954\\ 14.1451\\ 30.5325\\ 156.641\\ 7.6684\\ 15.3952\\ 28.3901\\ 142.7522\\ \hline \end{array} \\ \begin{array}{c} B\\ \hline \hline \\ \hline $	1.9019 3.1270 15.3322 1.4012 2.1094 4.4406 19.0963 1.3629 2.1455 3.8966 16.3336 old indicated the sn <b>2.9: EMSEs for v</b> <b>c</b> <sub>2</sub> 1.6494 2.8947 3.8033 26.6251 1.3819	$\begin{array}{c} 6.6739\\ 35.2562\\ 2.4713\\ 3.8912\\ 8.6451\\ 42.8419\\ 2.2028\\ 4.5035\\ 7.9984\\ 39.3749\\ \hline \\ abler EMSE\\ \hline \\ \hline$	$\begin{array}{c} 6.1911\\ 36.1952\\ 2.4747\\ 3.9483\\ 8.6224\\ 43.4421\\ 2.3043\\ 5.0588\\ 8.1217\\ 41.3574\\ \hline \\ \hline$	$\begin{array}{c} 3.1166\\ 15.2779\\ 1.3993\\ 2.1058\\ 4.4303\\ 19.0511\\ 1.3616\\ 2.1426\\ 3.8902\\ 16.3061\\ \hline \\ \hline$	$\begin{array}{c} 5.3999\\ 8.7935\\ 42.0009\\ 3.3992\\ 5.2536\\ 11.1534\\ 56.3899\\ 3.1764\\ 6.1252\\ 10.5169\\ 51.0804\\ \hline \end{array}$
200 n 50	$\begin{array}{c} 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ \hline\\ \rho^2\\ \hline\\ 0.8\\ 0.9\\ 0.95\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.8\\ 0.9\\ 0.8\\ 0.9\\ 0.8\\ 0.9\\ 0.9\\ 0.8\\ 0.9\\ \hline\end{array}$	15.27 27.2705 131.5003 8.9205 14.1834 30.6178 157.0304 7.6837 15.4263 28.4487 143.018 MLE 18.2156 30.5285 57.0240 315.518 11.8646 20.4850	15.1989 27.1466 131.0075 8.8954 14.1451 30.5325 156.641 7.6684 15.3952 28.3901 142.7522 B <b>Table</b> <u>C1</u> 17.8366 29.9479 56.0273 312.7813 11.7589 20.3032	1.9019 3.1270 15.3322 1.4012 2.1094 4.4406 19.0963 1.3629 2.1455 3.8966 16.3336 old indicated the sn <b>2 9: EMSEs for v</b> <b>c</b> <sub>2</sub> 1.6494 2.8947 3.8033 26.6251 1.3819 2.2728	$\begin{array}{c} 6.6739\\ 35.2562\\ 2.4713\\ 3.8912\\ 8.6451\\ 42.8419\\ 2.2028\\ 4.5035\\ 7.9984\\ 39.3749\\ \hline \\ 39.3749\\ \hline \\ \text{maller EMSE}\\ \hline \\ r=1 \text{ and } p=9\\ \hline \\ \hline$	$\begin{array}{c} 6.1911\\ 36.1952\\ 2.4747\\ 3.9483\\ 8.6224\\ 43.4421\\ 2.3043\\ 5.0588\\ 8.1217\\ 41.3574\\ \hline \\ \hline$	$\begin{array}{c} 3.1166\\ 15.2779\\ 1.3993\\ 2.1058\\ 4.4303\\ 19.0511\\ 1.3616\\ 2.1426\\ 3.8902\\ 16.3061\\ \hline \end{array}$	$\begin{array}{c} 5.3999\\ 8.7935\\ 42.0009\\ 3.3992\\ 5.2536\\ 11.1534\\ 56.3899\\ 3.1764\\ 6.1252\\ 10.5169\\ 51.0804\\ \hline \end{array}$
200 n 50	$\begin{array}{c} 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ \hline \end{array}$	15.27 27.2705 131.5003 8.9205 14.1834 30.6178 157.0304 7.6837 15.4263 28.4487 143.018 MLE 18.2156 30.5285 57.0240 315.518 11.8646 20.4850 37.6053	15.1989 27.1466 131.0075 8.8954 14.1451 30.5325 156.641 7.6684 15.3952 28.3901 142.7522 B <b>Table</b> <u>C1</u> 17.8366 29.9479 56.0273 312.7813 11.7589 20.3032 37.2942	1.9019 3.1270 15.3322 1.4012 2.1094 4.4406 19.0963 1.3629 2.1455 3.8966 16.3336 old indicated the sn <b>2 9: EMSEs for v</b> <b>2 (1)</b> <b>2 (1)</b> <b>2 (1)</b> <b>2 (1)</b> <b>2 (1)</b> <b>3 (</b>	$\begin{array}{c} 6.6739\\ 35.2562\\ 2.4713\\ 3.8912\\ 8.6451\\ 42.8419\\ 2.2028\\ 4.5035\\ 7.9984\\ 39.3749\\ \hline \\ \textbf{mathematical}\\ mathematical$	$\begin{array}{c} 6.1911\\ 36.1952\\ 2.4747\\ 3.9483\\ 8.6224\\ 43.4421\\ 2.3043\\ 5.0588\\ 8.1217\\ 41.3574\\ \hline \\ \hline$	$\begin{array}{c} 3.1166\\ 15.2779\\ 1.3993\\ 2.1058\\ 4.4303\\ 19.0511\\ 1.3616\\ 2.1426\\ 3.8902\\ 16.3061\\ \hline \\ \hline$	$\begin{array}{c} 5.3999\\ 8.7935\\ 42.0009\\ 3.3992\\ 5.2536\\ 11.1534\\ 56.3899\\ 3.1764\\ 6.1252\\ 10.5169\\ 51.0804\\ \hline \end{array}$
200 n 50	$\begin{array}{c} 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ \hline\\ \rho^2\\ \hline\\ 0.8\\ 0.9\\ 0.95\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.8\\ 0.9\\ 0.8\\ 0.9\\ 0.8\\ 0.9\\ 0.9\\ 0.8\\ 0.9\\ \hline\end{array}$	15.27 27.2705 131.5003 8.9205 14.1834 30.6178 157.0304 7.6837 15.4263 28.4487 143.018	15.1989 27.1466 131.0075 8.8954 14.1451 30.5325 156.641 7.6684 15.3952 28.3901 142.7522 B <b>Table</b> <u>C<sub>1</sub></u> 17.8366 29.9479 56.0273 312.7813 11.7589 20.3032 37.2942 185.8586	1.9019 3.1270 15.3322 1.4012 2.1094 4.4406 19.0963 1.3629 2.1455 3.8966 16.3336 old indicated the sn <b>2 9: EMSEs for v</b> <b>c</b> <sub>2</sub> 1.6494 2.8947 3.8033 26.6251 1.3819 2.2728	$\begin{array}{c} 6.6739\\ 35.2562\\ 2.4713\\ 3.8912\\ 8.6451\\ 42.8419\\ 2.2028\\ 4.5035\\ 7.9984\\ 39.3749\\ \text{maller EMSE}\\ \hline = 1 \text{ and } p=9\\ \hline compse\\ \hline c_3\\ \hline c_3\\ \hline c_3\\ \hline c_3\\ \hline c_3\\ \hline c_4574\\ 11.2609\\ 69.7525\\ 2.6686\\ 4.7265\\ 7.9611\\ 38.9949\\ \end{array}$	$\begin{array}{c} 6.1911\\ 36.1952\\ 2.4747\\ 3.9483\\ 8.6224\\ 43.4421\\ 2.3043\\ 5.0588\\ 8.1217\\ 41.3574\\ \hline \\ \hline$	$\begin{array}{c} 3.1166\\ 15.2779\\ 1.3993\\ 2.1058\\ 4.4303\\ 19.0511\\ 1.3616\\ 2.1426\\ 3.8902\\ 16.3061\\ \hline \end{array}$	$\begin{array}{c} 5.3999\\ 8.7935\\ 42.0009\\ 3.3992\\ 5.2536\\ 11.1534\\ 56.3899\\ 3.1764\\ 6.1252\\ 10.5169\\ 51.0804\\ \hline \end{array}$
200 <u>n</u> 50 100	$\begin{array}{c} 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ \hline \end{array}$	15.27 27.2705 131.5003 8.9205 14.1834 30.6178 157.0304 7.6837 15.4263 28.4487 143.018 MLE 18.2156 30.5285 57.0240 315.518 11.8646 20.4850 37.6053	15.1989 27.1466 131.0075 8.8954 14.1451 30.5325 156.641 7.6684 15.3952 28.3901 142.7522 B <b>Table</b> <u>C1</u> 17.8366 29.9479 56.0273 312.7813 11.7589 20.3032 37.2942	1.9019 3.1270 15.3322 1.4012 2.1094 4.4406 19.0963 1.3629 2.1455 3.8966 16.3336 old indicated the sn <b>2 9: EMSEs for v</b> <b>2 (1)</b> <b>2 (1)</b> <b>2 (1)</b> <b>2 (1)</b> <b>2 (1)</b> <b>3 (</b>	$\begin{array}{c} 6.6739\\ 35.2562\\ 2.4713\\ 3.8912\\ 8.6451\\ 42.8419\\ 2.2028\\ 4.5035\\ 7.9984\\ 39.3749\\ \text{maller EMSE}\\ \hline = 1 \text{ and } p=9\\ \hline compse\\ \hline c_3\\ \hline c_3\\ \hline c_3\\ \hline c_3\\ \hline c_3\\ \hline c_4574\\ 11.2609\\ 69.7525\\ 2.6686\\ 4.7265\\ 7.9611\\ 38.9949\\ \end{array}$	$\begin{array}{c} 6.1911\\ 36.1952\\ 2.4747\\ 3.9483\\ 8.6224\\ 43.4421\\ 2.3043\\ 5.0588\\ 8.1217\\ 41.3574\\ \hline \\ \hline$	$\begin{array}{c} 3.1166\\ 15.2779\\ 1.3993\\ 2.1058\\ 4.4303\\ 19.0511\\ 1.3616\\ 2.1426\\ 3.8902\\ 16.3061\\ \hline \\ \hline$	$\begin{array}{c} 5.3999\\ 8.7935\\ 42.0009\\ 3.3992\\ 5.2536\\ 11.1534\\ 56.3899\\ 3.1764\\ 6.1252\\ 10.5169\\ 51.0804\\ \hline \end{array}$
200 <u>n</u> 50 100	$\begin{array}{c} 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ \end{array}$	15.27 27.2705 131.5003 8.9205 14.1834 30.6178 157.0304 7.6837 15.4263 28.4487 143.018	15.1989 27.1466 131.0075 8.8954 14.1451 30.5325 156.641 7.6684 15.3952 28.3901 142.7522 B <b>Table</b> <u>C1</u> 17.8366 29.9479 56.0273 312.7813 11.7589 20.3032 37.2942 185.8586 12.2252	1.9019 3.1270 15.3322 1.4012 2.1094 4.4406 19.0963 1.3629 2.1455 3.8966 16.3336 old indicated the sn <b>9: EMSEs for 1</b> <b>c</b> <sub>2</sub> 1.6494 2.8947 3.8033 26.6251 1.3819 2.2728 3.2184 14.221 1.6152	$\begin{array}{c} 6.6739\\ 35.2562\\ 2.4713\\ 3.8912\\ 8.6451\\ 42.8419\\ 2.2028\\ 4.5035\\ 7.9984\\ 39.3749\\ \text{mailer EMSE}\\ \hline = 1 \text{ and } p=9\\ \hline comPSE\\ \hline c_3\\ \hline c_3\\ \hline c_3\\ \hline c_3\\ \hline c_3\\ \hline c_3\\ \hline c_686\\ 4.7265\\ 7.9611\\ 38.9949\\ 3.0121\\ \end{array}$	$\begin{array}{c} 6.1911\\ 36.1952\\ 2.4747\\ 3.9483\\ 8.6224\\ 43.4421\\ 2.3043\\ 5.0588\\ 8.1217\\ 41.3574\\ \hline \\ \hline$	$\begin{array}{c} 3.1166\\ 15.2779\\ 1.3993\\ 2.1058\\ 4.4303\\ 19.0511\\ 1.3616\\ 2.1426\\ 3.8902\\ 16.3061\\ \hline \end{array}$	$\begin{array}{c} 5.3999\\ 8.7935\\ 42.0009\\ 3.3992\\ 5.2536\\ 11.1534\\ 56.3899\\ 3.1764\\ 6.1252\\ 10.5169\\ 51.0804\\ \hline \end{array}$
200 <u>n</u> 50 100	$\begin{array}{c} 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.95\\ 0.99\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.9\\ 0.9\\ 0.9\\ 0.9\\ 0.9\\ 0.9\\ 0.9$	15.27 27.2705 131.5003 8.9205 14.1834 30.6178 157.0304 7.6837 15.4263 28.4487 143.018	15.1989 27.1466 131.0075 8.8954 14.1451 30.5325 156.641 7.6684 15.3952 28.3901 142.7522 B Table C1 17.8366 29.9479 56.0273 312.7813 11.7589 20.3032 37.2942 185.8586 12.2252 21.6253	1.9019 3.1270 15.3322 1.4012 2.1094 4.4406 19.0963 1.3629 2.1455 3.8966 16.3336 old indicated the sn <b>2.9: EMSEs for v</b> <b>2.9: EMSEs for v</b> <b>2.8947</b> 3.8033 26.6251 1.3819 2.2728 3.2184 14.221 1.6152 2.4081	$\begin{array}{r} 6.6739\\ 35.2562\\ 2.4713\\ 3.8912\\ 8.6451\\ 42.8419\\ 2.2028\\ 4.5035\\ 7.9984\\ 39.3749\\ \hline \end{array}$ haller EMSE $\begin{array}{r} = 1 \text{ and } p=9\\ \hline \hline \\ COMPSE\\ \hline \hline \\ c_3\\ 3.5982\\ 6.4574\\ 11.2609\\ 69.7525\\ 2.6686\\ 4.7265\\ 7.9611\\ 38.9949\\ 3.0121\\ 4.9657\\ \end{array}$	$\begin{array}{c} 6.1911\\ 36.1952\\ 2.4747\\ 3.9483\\ 8.6224\\ 43.4421\\ 2.3043\\ 5.0588\\ 8.1217\\ 41.3574\\ \hline \\ \hline$	$\begin{array}{c} 3.1166\\ 15.2779\\ 1.3993\\ 2.1058\\ 4.4303\\ 19.0511\\ 1.3616\\ 2.1426\\ 3.8902\\ 16.3061\\ \hline \\ \hline$	$\begin{array}{c} 5.3999\\ 8.7935\\ 42.0009\\ 3.3992\\ 5.2536\\ 11.1534\\ 56.3899\\ 3.1764\\ 6.1252\\ 10.5169\\ 51.0804\\ \hline \end{array}$
200 <u>n</u> 50 100	$\begin{array}{c} 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.95\\ 0.99\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.9$	15.27 27.2705 131.5003 8.9205 14.1834 30.6178 157.0304 7.6837 15.4263 28.4487 143.018	15.1989 27.1466 131.0075 8.8954 14.1451 30.5325 156.641 7.6684 15.3952 28.3901 142.7522 B Table C <sub>1</sub> 17.8366 29.9479 56.0273 312.7813 11.7589 20.3032 37.2942 185.8586 12.2252 21.6253 42.9662	1.9019 3.1270 15.3322 1.4012 2.1094 4.4406 19.0963 1.3629 2.1455 3.8966 16.3336 old indicated the sn <b>2.9: EMSEs for v</b> <b>c</b> <sub>2</sub> 1.6494 2.8947 3.8033 26.6251 1.3819 2.2728 3.2184 14.221 1.6152 2.4081 4.2817	$\begin{array}{c} 6.6739\\ 35.2562\\ 2.4713\\ 3.8912\\ 8.6451\\ 42.8419\\ 2.2028\\ 4.5035\\ 7.9984\\ 39.3749\\ \hline \\ \textbf{mailer EMSE}\\ $	$\begin{array}{c} 6.1911\\ 36.1952\\ 2.4747\\ 3.9483\\ 8.6224\\ 43.4421\\ 2.3043\\ 5.0588\\ 8.1217\\ 41.3574\\ \hline \\ \hline$	$\begin{array}{c} 3.1166\\ 15.2779\\ 1.3993\\ 2.1058\\ 4.4303\\ 19.0511\\ 1.3616\\ 2.1426\\ 3.8902\\ 16.3061\\ \hline \end{array}$	$\begin{array}{c} 5.3999\\ 8.7935\\ 42.0009\\ 3.3992\\ 5.2536\\ 11.1534\\ 56.3899\\ 3.1764\\ 6.1252\\ 10.5169\\ 51.0804\\ \hline \end{array}$
200 <u>n</u> 50 100 150	$\rho^{2} = \frac{\rho^{2}}{0.8}$	15.27 27.2705 131.5003 8.9205 14.1834 30.6178 157.0304 7.6837 15.4263 28.4487 143.018	$\begin{array}{c} 15.1989\\ 27.1466\\ 131.0075\\ 8.8954\\ 14.1451\\ 30.5325\\ 156.641\\ 7.6684\\ 15.3952\\ 28.3901\\ 142.7522\\ \end{array}$	1.9019 3.1270 15.3322 1.4012 2.1094 4.4406 19.0963 1.3629 2.1455 3.8966 16.3336 old indicated the sn <b>2 9:</b> EMSEs for $v$ <b>2</b> <b>1.6494</b> 2.8947 3.8033 26.6251 1.3819 2.2728 3.2184 14.221 1.6152 2.4081 4.2817 16.1405	$\begin{array}{c} 6.6739\\ 35.2562\\ 2.4713\\ 3.8912\\ 8.6451\\ 42.8419\\ 2.2028\\ 4.5035\\ 7.9984\\ 39.3749\\ \hline \end{array}$ haller EMSE $\begin{array}{c} r=1 \text{ and } p=9\\ \hline \hline comPSE\\ \hline c_3\\ 3.5982\\ 6.4574\\ 11.2609\\ 69.7525\\ 2.6686\\ 4.7265\\ 7.9611\\ 38.9949\\ 3.0121\\ 4.9657\\ 10.0226\\ 47.3655\\ \end{array}$	$\begin{array}{c} 6.1911\\ 36.1952\\ 2.4747\\ 3.9483\\ 8.6224\\ 43.4421\\ 2.3043\\ 5.0588\\ 8.1217\\ 41.3574\\ \hline \\ \hline$	$\begin{array}{c} 3.1166\\ 15.2779\\ 1.3993\\ 2.1058\\ 4.4303\\ 19.0511\\ 1.3616\\ 2.1426\\ 3.8902\\ 16.3061\\ \hline \end{array}$	$\begin{array}{c} 5.3999\\ 8.7935\\ 42.0009\\ 3.3992\\ 5.2536\\ 11.1534\\ 56.3899\\ 3.1764\\ 6.1252\\ 10.5169\\ 51.0804\\ \hline \end{array}$
200 <u>n</u> 50 100 150	$\begin{array}{c} 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.95\\ 0.99\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.9$	15.27 27.2705 131.5003 8.9205 14.1834 30.6178 157.0304 7.6837 15.4263 28.4487 143.018	15.1989 27.1466 131.0075 8.8954 14.1451 30.5325 156.641 7.6684 15.3952 28.3901 142.7522 B Table C <sub>1</sub> 17.8366 29.9479 56.0273 312.7813 11.7589 20.3032 37.2942 185.8586 12.2252 21.6253 42.9662	1.9019 3.1270 15.3322 1.4012 2.1094 4.4406 19.0963 1.3629 2.1455 3.8966 16.3336 old indicated the sn <b>2.9: EMSEs for v</b> <b>c</b> <sub>2</sub> 1.6494 2.8947 3.8033 26.6251 1.3819 2.2728 3.2184 14.221 1.6152 2.4081 4.2817	$\begin{array}{c} 6.6739\\ 35.2562\\ 2.4713\\ 3.8912\\ 8.6451\\ 42.8419\\ 2.2028\\ 4.5035\\ 7.9984\\ 39.3749\\ \hline \\ \textbf{mailer EMSE}\\ $	$\begin{array}{c} 6.1911\\ 36.1952\\ 2.4747\\ 3.9483\\ 8.6224\\ 43.4421\\ 2.3043\\ 5.0588\\ 8.1217\\ 41.3574\\ \hline \\ \hline$	$\begin{array}{c} 3.1166\\ 15.2779\\ 1.3993\\ 2.1058\\ 4.4303\\ 19.0511\\ 1.3616\\ 2.1426\\ 3.8902\\ 16.3061\\ \hline \end{array}$	$\begin{array}{c} 5.3999\\ 8.7935\\ 42.0009\\ 3.3992\\ 5.2536\\ 11.1534\\ 56.3899\\ 3.1764\\ 6.1252\\ 10.5169\\ 51.0804\\ \hline \end{array}$
200 <u>n</u> 50 100 150	$\begin{array}{c} 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.95\\ 0.99\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.99\\ 0.8\\ 0.9\\ 0.9\\ 0.99\\ 0.8\\ 0.9\\ 0.99\\ 0.8\\ 0.9\\ 0.99\\ 0.8\\ 0.9\\ 0.9\\ 0.9\\ 0.9\\ 0.9\\ 0.9\\ 0.9\\ 0.9$	15.27 27.2705 131.5003 8.9205 14.1834 30.6178 157.0304 7.6837 15.4263 28.4487 143.018 MLE 18.2156 30.5285 57.0240 315.518 11.8646 20.4850 37.6053 186.9961 12.2911 21.7443 43.2059 211.1366 10.7101	15.1989 27.1466 131.0075 8.8954 14.1451 30.5325 156.641 7.6684 15.3952 28.3901 142.7522 B <b>Table</b> C1 17.8366 29.9479 56.0273 312.7813 11.7589 20.3032 37.2942 185.8586 12.2252 21.6253 42.9662 210.2504 10.6662	1.9019 3.1270 15.3322 1.4012 2.1094 4.4406 19.0963 1.3629 2.1455 3.8966 16.3336 old indicated the sn <b>2 9: EMSEs for v</b> <b>2</b> <b>1</b> .6494 2.8947 3.8033 26.6251 1.3819 2.2728 3.2184 14.221 1.6152 2.4081 4.2817 16.1405 1.4143	$\begin{array}{c} 6.6739\\ 35.2562\\ 2.4713\\ 3.8912\\ 8.6451\\ 42.8419\\ 2.2028\\ 4.5035\\ 7.9984\\ 39.3749\\ \hline \end{array}$ haller EMSE $\begin{array}{c} r=1 \text{ and } p=9\\ \hline \hline \\ COMPSE\\ \hline c_3\\ \hline 3.5982\\ 6.4574\\ 11.2609\\ 69.7525\\ 2.6686\\ 4.7265\\ 7.9611\\ 38.9949\\ 3.0121\\ 4.9657\\ 10.0226\\ 47.3655\\ 2.6393\\ \end{array}$	$\begin{array}{c} 6.1911\\ 36.1952\\ 2.4747\\ 3.9483\\ 8.6224\\ 43.4421\\ 2.3043\\ 5.0588\\ 8.1217\\ 41.3574\\ \hline \\ \hline$	$\begin{array}{c} 3.1166\\ 15.2779\\ 1.3993\\ 2.1058\\ 4.4303\\ 19.0511\\ 1.3616\\ 2.1426\\ 3.8902\\ 16.3061\\ \hline \end{array}$	$\begin{array}{c} 5.3999\\ 8.7935\\ 42.0009\\ 3.3992\\ 5.2536\\ 11.1534\\ 56.3899\\ 3.1764\\ 6.1252\\ 10.5169\\ 51.0804\\ \hline \end{array}$
200 <u>n</u> 50 100 150	$\begin{array}{c} 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.95\\ 0.99\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.9\\ 0.9\\ 0.8\\ 0.9\\ 0.9\\ 0.9\\ 0.8\\ 0.9\\ 0.9\\ 0.8\\ 0.9\\ 0.9\\ 0.8\\ 0.9\\ 0.9\\ 0.8\\ 0.9\\ 0.9\\ 0.8\\ 0.9\\ 0.9\\ 0.8\\ 0.9\\ 0.9\\ 0.8\\ 0.9\\ 0.9\\ 0.8\\ 0.9\\ 0.9\\ 0.8\\ 0.9\\ 0.9\\ 0.8\\ 0.9\\ 0.9\\ 0.8\\ 0.9\\ 0.9\\ 0.8\\ 0.9\\ 0.9\\ 0.9\\ 0.8\\ 0.9\\ 0.9\\ 0.9\\ 0.8\\ 0.9\\ 0.9\\ 0.9\\ 0.9\\ 0.8\\ 0.9\\ 0.9\\ 0.9\\ 0.8\\ 0.9\\ 0.9\\ 0.9\\ 0.9\\ 0.8\\ 0.9\\ 0.9\\ 0.9\\ 0.9\\ 0.9\\ 0.9\\ 0.9\\ 0.9$	15.27 27.2705 131.5003 8.9205 14.1834 30.6178 157.0304 7.6837 15.4263 28.4487 143.018 MLE 18.2156 30.5285 57.0240 315.518 11.8646 20.4850 37.6053 186.9961 12.2911 21.7443 43.2059 211.1366 10.7101 20.8369	15.1989 27.1466 131.0075 8.8954 14.1451 30.5325 156.641 7.6684 15.3952 28.3901 142.7522 B Table C1 17.8366 29.9479 56.0273 312.7813 11.7589 20.3032 37.2942 185.8586 12.2252 21.6253 42.9662 210.2504 10.6662 20.7545	$\begin{array}{c} 1.9019\\ 3.1270\\ 15.3322\\ 1.4012\\ 2.1094\\ 4.4406\\ 19.0963\\ 1.3629\\ 2.1455\\ 3.8966\\ 16.3336\\ 0 d indicated the sn\\ 2 9: EMSEs for v\\ \hline c_2\\ \hline c_2\\ \hline 1.6494\\ 2.8947\\ 3.8033\\ 26.6251\\ 1.3819\\ 2.2728\\ 3.2184\\ 14.221\\ 1.6152\\ 2.4081\\ 4.2817\\ 16.1405\\ 1.4143\\ 2.4984\\ \hline \end{array}$	$\begin{array}{c} 6.6739\\ 35.2562\\ 2.4713\\ 3.8912\\ 8.6451\\ 42.8419\\ 2.2028\\ 4.5035\\ 7.9984\\ 39.3749\\ \hline \end{array}$ haller EMSE $\begin{array}{c} r=1 \mbox{ and } p=9\\ \hline \mbox{ COMPSE}\\ \hline c_3\\ \hline \mbox{ compSE}\\ \hline c_3\\ \hline \mbox{ compSE}\\ \hline c_6866\\ 4.7265\\ 7.9611\\ 38.9949\\ 3.0121\\ 4.9657\\ 10.0226\\ 47.3655\\ 2.66393\\ 5.1755\\ \end{array}$	$\begin{array}{c} 6.1911\\ 36.1952\\ 2.4747\\ 3.9483\\ 8.6224\\ 43.4421\\ 2.3043\\ 5.0588\\ 8.1217\\ 41.3574\\ \hline \end{array}$	$\begin{array}{c} 3.1166\\ 15.2779\\ 1.3993\\ 2.1058\\ 4.4303\\ 19.0511\\ 1.3616\\ 2.1426\\ 3.8902\\ 16.3061\\ \hline \end{array}$	5.3999 8.7935 42.0009 3.3992 5.2536 11.1534 56.3899 3.1764 6.1252 10.5169 51.0804 $c_6$ 4.1569 7.1828 12.9065 72.2782 3.6635 5.5805 9.1454 42.4321 3.8892 5.9018 11.6322 55.2976 3.3266 6.3813
200 n	$\begin{array}{c} 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.95\\ 0.99\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.99\\ 0.8\\ 0.9\\ 0.9\\ 0.99\\ 0.8\\ 0.9\\ 0.99\\ 0.8\\ 0.9\\ 0.99\\ 0.8\\ 0.9\\ 0.9\\ 0.9\\ 0.9\\ 0.9\\ 0.9\\ 0.9\\ 0.9$	15.27 27.2705 131.5003 8.9205 14.1834 30.6178 157.0304 7.6837 15.4263 28.4487 143.018 MLE 18.2156 30.5285 57.0240 315.518 11.8646 20.4850 37.6053 186.9961 12.2911 21.7443 43.2059 211.1366 10.7101	15.1989 27.1466 131.0075 8.8954 14.1451 30.5325 156.641 7.6684 15.3952 28.3901 142.7522 B <b>Table</b> C1 17.8366 29.9479 56.0273 312.7813 11.7589 20.3032 37.2942 185.8586 12.2252 21.6253 42.9662 210.2504 10.6662	1.9019 3.1270 15.3322 1.4012 2.1094 4.4406 19.0963 1.3629 2.1455 3.8966 16.3336 old indicated the sn <b>2 9: EMSEs for v</b> <b>2</b> <b>1</b> .6494 2.8947 3.8033 26.6251 1.3819 2.2728 3.2184 14.221 1.6152 2.4081 4.2817 16.1405 1.4143	$\begin{array}{c} 6.6739\\ 35.2562\\ 2.4713\\ 3.8912\\ 8.6451\\ 42.8419\\ 2.2028\\ 4.5035\\ 7.9984\\ 39.3749\\ \hline \end{array}$ haller EMSE $\begin{array}{c} r=1 \text{ and } p=9\\ \hline \hline \\ COMPSE\\ \hline c_3\\ \hline 3.5982\\ 6.4574\\ 11.2609\\ 69.7525\\ 2.6686\\ 4.7265\\ 7.9611\\ 38.9949\\ 3.0121\\ 4.9657\\ 10.0226\\ 47.3655\\ 2.6393\\ \end{array}$	$\begin{array}{c} 6.1911\\ 36.1952\\ 2.4747\\ 3.9483\\ 8.6224\\ 43.4421\\ 2.3043\\ 5.0588\\ 8.1217\\ 41.3574\\ \hline \\ \hline$	$\begin{array}{c} 3.1166\\ 15.2779\\ 1.3993\\ 2.1058\\ 4.4303\\ 19.0511\\ 1.3616\\ 2.1426\\ 3.8902\\ 16.3061\\ \hline \end{array}$	$\begin{array}{c} 5.3999\\ 8.7935\\ 42.0009\\ 3.3992\\ 5.2536\\ 11.1534\\ 56.3899\\ 3.1764\\ 6.1252\\ 10.5169\\ 51.0804\\ \hline \end{array}$

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		Table	<b>10:</b> EMSEs for 1	v = 1.25  and  p =	9	
$\rho^2$				COMPSE		
	MLE	<i>C</i> <sub>1</sub>	<i>C</i> <sub>2</sub>	<i>C</i> <sub>3</sub>	$C_4$	<i>C</i> <sub>5</sub>
0.8	29.8120	28.5768	2.1102	4.9335	3.9226	2.0495
0.9	50.7526	48.7797	3.0771	8.8107	7.1843	2.9813
0.95	100.4128	97.1939	4.7484	16.3670	11.1816	4.6287
0.99	519.9196	508.1721	29.7907	94.2948	70.3630	29.2287
0.8 0.9	16.2607 28.8359	15.9571 28.2972	1.3567 2.0835	2.8967 4.9465	2.5253 3.8663	1.3465 2.0596
0.9	62.6879	61.5431	4.0800	11.3018	8.7442	4.0185
0.99	270.8632	267.4712	14.0441	45.1085	30.6100	13.8882
0.8	18.4796	18.2584	1.6304	3.4844	2.8335	1.6202
0.9	31.2447	30.8644	2.3371	5.6250	4.3683	2.3175
0.95	70.0785	69.2906	4.5931	13.0057	9.7575	4.5503
0.99	317.0939	314.1604	23.3084	62.8703	51.9734	23.1080
0.8	17.3403	17.1807	1.6261	3.3796	2.9540	1.6183
0.9	35.0910	34.7739	2.6425	6.9631	6.3796	2.6259
0.95	59.5165	58.9942	4.4078	11.3089	9.3730	4.3775
0.99	309.805	307.907	19.1649	60.9199	46.9694	19.0453
			Bold indicated the s	maller EMSE		
		Table 1	1: EMSEs for v	= 0.85 and $p=2$	12	
2		Tuble		COMPSE	14	
$ ho^2$ .	MLE	<i>c</i> <sub>1</sub>	<i>C</i> <sub>2</sub>	C3	$c_4$	<i>C</i> <sub>5</sub>
0.8	30.2268	29.8619	2.0519	5.7249	4.8988	2.0369
0.9	55.9570	55.3580	5.0961	11.8682	11.5056	5.0562
0.95	130.3971	129.061	11.1001	30.1568	28.5111	11.0038
0.99	530.9519	527.7231	36.4428	107.1048	102.876	36.2200
0.8	11.6471	11.5917	1.4046	2.6799	2.7015	1.4014
0.9	21.8890	21.7877	2.4383	5.0299	4.7187	2.4306
0.95	43.0677	42.8641	3.8081	9.3312	8.7583	3.7942
0.99	217.66	216.93	18.5146	50.4187	53.1009	18.4600
0.8	11.6700	11.6357	1.6905	3.1125	3.3012	1.6876
0.9	20.1339	20.0777	2.2421	4.9004	4.9984	2.2381
0.95 0.99	41.8159 176.3168	41.6944 175.9053	4.1354 17.5253	9.7494 42.9961	9.8362 44.5394	4.1259 17.4879
0.99	9.3094	9.2902	1.3341	2.3564	2.3524	1.3329
0.8	17.8146	17.7792	2.0370	4.5573	4.7551	2.0345
0.95	34.6227	34.5528	3.4577	8.2844	8.4306	3.4523
0.99	156.448	156.193	15.5181	38.1152	38.2063	15.4951
			Bold indicated the s			
		m 11	<b>40</b> EMCE (	4 1 40		
		Table	<b>12:</b> EMSES for	v = 1 and $p = 12$	2	
$\rho^2$ -	MLE	C	6	COMPSE	6	6
0.8	48.5934	<i>c</i> <sub>1</sub> 47.4954	$\frac{c_2}{3.3632}$	<i>c</i> <sub>3</sub> 8.7121	$\frac{c_4}{8.2088}$	<i>c</i> <sub>5</sub> <b>3.3029</b>
0.9	77.4855	76.0530	4.4443	13.4171	11.6011	4.3811
0.95	150.571	147.9989	8.2944	28.4764	29.9445	8.1640
0.99	800.6394	793.2687	47.6374	145.4789	125.4188	47.1892
0.8	16.4466	16.3000	1.6439	3.4035	3.1997	1.6362
0.9	33.5598	33.2668	2.4338	6.5862	6.0150	2.4192
0.95	62.0426	61.5142	4.5741	12.1235	10.3679	4.5423
0.99	318.6942	316.7213	17.0613	57.4023	47.2060	16.9632
0.8	15.8929	15.8042	1.4558	3.2192	3.0713	1.4521
0.9	27.6453	27.4919	2.3008	5.3943	4.8452	2.2922
0.95	55.3014	54.9955	3.9494	10.5169	8.3756	3.9326
0.99	277.5442	276.3905	20.3704	55.6302	46.0304	20.2893
0.8	14.2363	14.1776	1.3940	2.9350	2.8181	1.3915
0.9	25.0326	24.9315	2.1893	5.0682	4.3449	2.1836
0.95	49.4963	49.2973	4.0990	10.3963	9.4561 49.0265	4.0858 18.4388
0.99	247.9527	247.1612	18.4930 Bold indicated the s	52.1994 maller EMSE	49.0205	10.4300

*c*<sub>6</sub> 5.1110 8.9824 14.7239

83.3667 3.0929 4.9256

11.0719 41.0175

41.0175 4.0118 5.7047 13.7462 61.9871

3.9643 7.9898

11.2819 65.999

с<sub>6</sub> 7.4582

14.1663 37.4655 120.1458 3.7111

6.9067 12.7959 66.7717

4.4215 7.0077 14.1508 57.3847 3.5667

3.5667 6.5408 11.7178 54.4191

*c*<sub>6</sub> 10.1686

15.7877 30.9811

30.9811 150.6116 4.3053 8.5112

 $\begin{array}{c} 13.8004 \\ 68.0070 \end{array}$ 

4.5957 7.096 13.9478 70.2910 4.0668

6.8289 13.5885 67.0262

п

50

100

150

200

п

50

100

150

200

п

50

100

150

200

**Table 13:** EMSEs for v = 1.25 and p=12

n	$\rho^2$	COMPSE						
n	ρ	MLE	<i>c</i> <sub>1</sub>	<i>C</i> <sub>2</sub>	<i>C</i> <sub>3</sub>	$c_4$	<i>C</i> <sub>5</sub>	C <sub>6</sub>
50	0.8	66.5138	64.0073	3.0372	9.7563	7.0821	2.9489	10.2700
	0.9	114.975	110.9237	6.1130	18.2827	14.9224	5.9085	16.9588
	0.95	225.1859	219.2014	8.7937	32.8742	22.2083	8.5763	28.9148
	0.99	1220.882	1201.324	46.8510	180.4798	139.0976	46.1052	146.2542
100	0.8	23.8395	23.4027	1.4939	3.4445	2.6202	1.4816	3.8261
	0.9	47.6500	46.7618	2.7865	7.4517	5.9284	2.7503	7.9167
	0.95	93.3668	91.8145	4.5054	14.0700	10.4409	4.4413	14.7955
	0.99	485.9481	481.4397	17.6006	73.2696	51.4461	17.4287	80.1791
150	0.8	22.8557	22.5772	1.3937	3.3526	2.6201	1.3870	3.9435
	0.9	42.4388	41.9304	2.2662	6.5493	4.9716	2.2484	7.7202
	0.95	87.6691	86.7035	4.3972	13.8002	9.6368	4.3614	15.7909
	0.99	394.6527	391.5111	19.5328	62.4182	49.1158	19.3725	67.6536
200	0.8	20.6514	20.4682	1.5539	3.4525	2.8835	1.5474	4.3300
	0.9	38.2561	37.9073	2.3842	6.4367	5.2434	2.3707	7.6864
	0.95	71.4081	70.7905	3.8656	11.0292	8.2573	3.8390	12.2316
	0.99	358.3625	355.8587	17.0435	58.2462	45.1041	16.9289	62.7291

Bold indicated the smaller EMSE

Table 14: Estimated COM Poisson regression coefficients and MSEs for plastic plywood data

Terms	MLE -	COMPSE					
	MLE	<i>c</i> <sub>1</sub>	<i>C</i> <sub>2</sub>	<i>C</i> <sub>3</sub>	$c_4$	c <sub>5</sub>	C <sub>6</sub>
Constant	1.4397	1.4393	0.5670	0.8577	1.2232	0.5668	0.4532
<i>x</i> <sub>1</sub>	0.4937	0.4936	0.1944	0.2941	0.4195	0.1944	0.1554
<i>x</i> <sub>2</sub>	0.6011	0.6009	0.2367	0.3581	0.5107	0.2367	0.1892
<i>x</i> <sub>3</sub>	0.3818	0.3817	0.1504	0.2275	0.3244	0.1503	0.1202
$x_4$	0.7401	0.7399	0.2915	0.4409	0.6288	0.2914	0.2330
MSE	6.7689	4.9352	3.5339	3.1553	5.3734	2.3767	2.3100

With a fixed sample size, explanatory variables, and dispersion parameter, the EMSEs of the COMPSE, using all proposed Stein parameters, were lower than those of the MLE. When the model included correlated regressors, the EMSE decreased sample size increased. Additionally, the as multicollinearity and the number of regressors directly affected the performance of the estimators. The EMSEs were lowest for overdispersion compared to underdispersion and equidispersion. Therefore, based on simulation and real application results, we conclude that our newly proposed estimator for the COMPRM is more appropriate than the MLE in the presence of multicollinearity and dispersion.

### **Compliance with ethical standards**

### **Conflict of interest**

The author(s) declared no potential conflicts of interest with respect to the research, authorship, and/or publication of this article.

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